

Three dimensional determination of etch track parameters in plastic nuclear track detectors: findings on bulk etch rate and implications for dosimetry.

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Summary and Conclusion

- Bulk etch rate in plastic detectors varies significantly
 - during etch time (CR 39)
 - locally by 10% to 25% (CR 39 and cellulose nitrate)
- Precision of dose equivalent measured thereby limited to perhaps 20% or more (neglecting other sources of error)

Overview

Historical background – motivation

2D measurement technique

3D measurement technique – experimental

3D measurement technique – theoretical analysis

3D measurements – accuracy/precision

Local bulk layer data (cellulose nitrate, D1 mission)

Local bulk layer data (CR 39, ISS mission/HIMAC)

Global bulk layer data (CR 39, ISS/HIMAC, mechanical thickness)

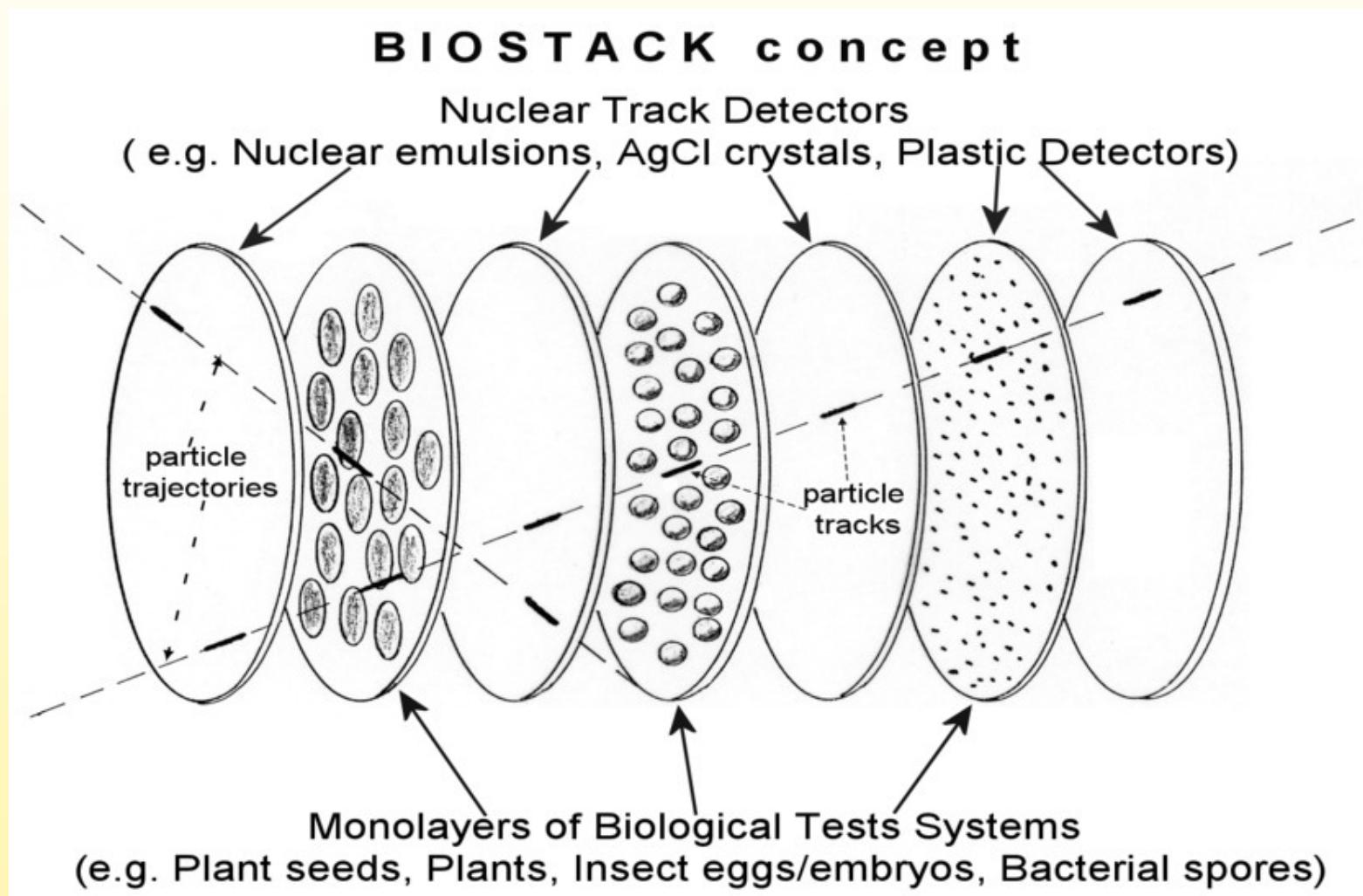
2D – 3D comparisons (CR 39)

Implications for dosimetry

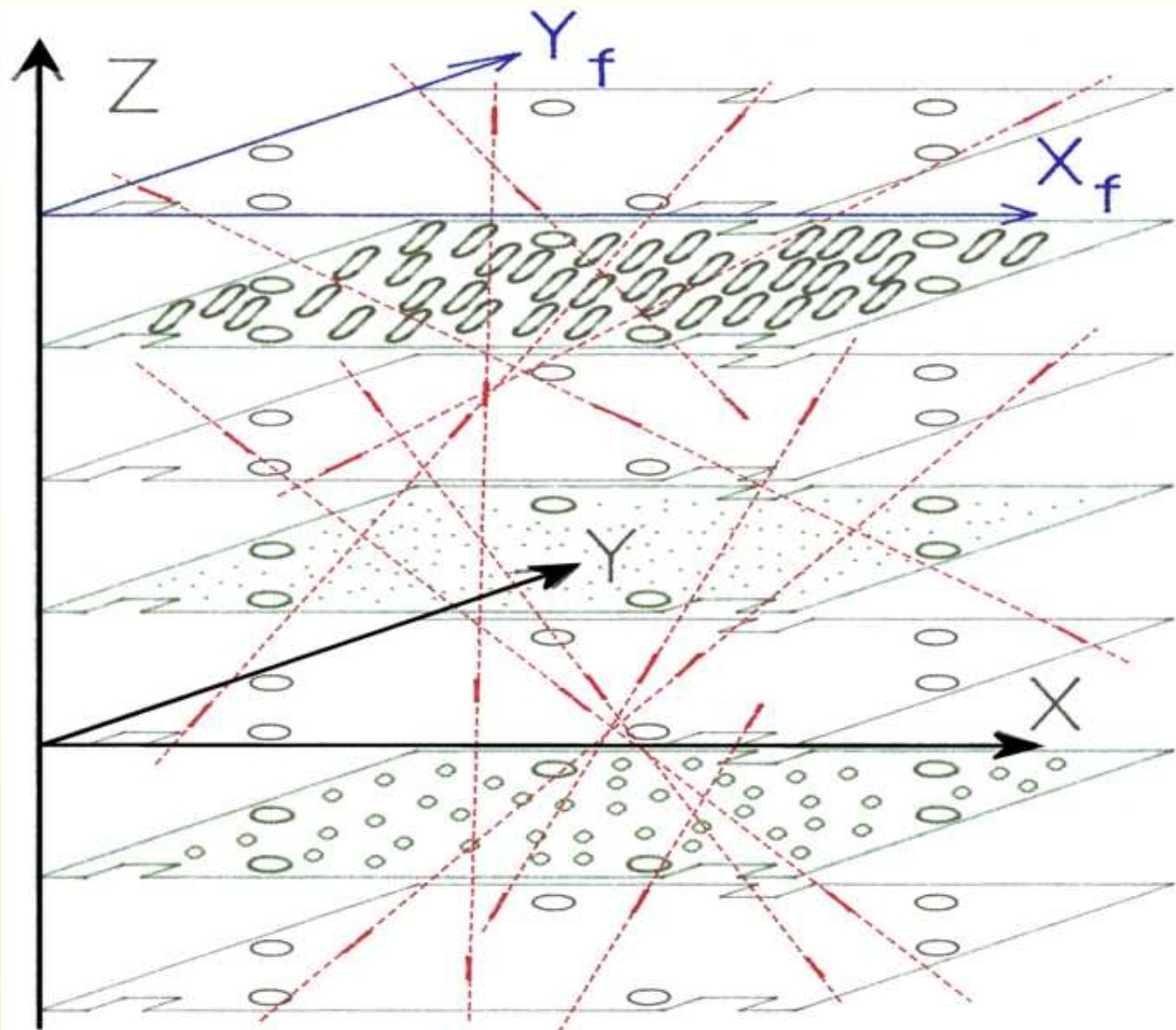
Puzzles (a few, for me)

Historical background – motivation

Background



Localization of particle tracks in biological test organisms



Co-ordinate systems involved in microscopic track measurements

X_S, Y_S :
Microscope
Stage System

X_f, Y_f :
Detector
Foil System



Y_S

X_T, Y_T : Etch Track System

X_S

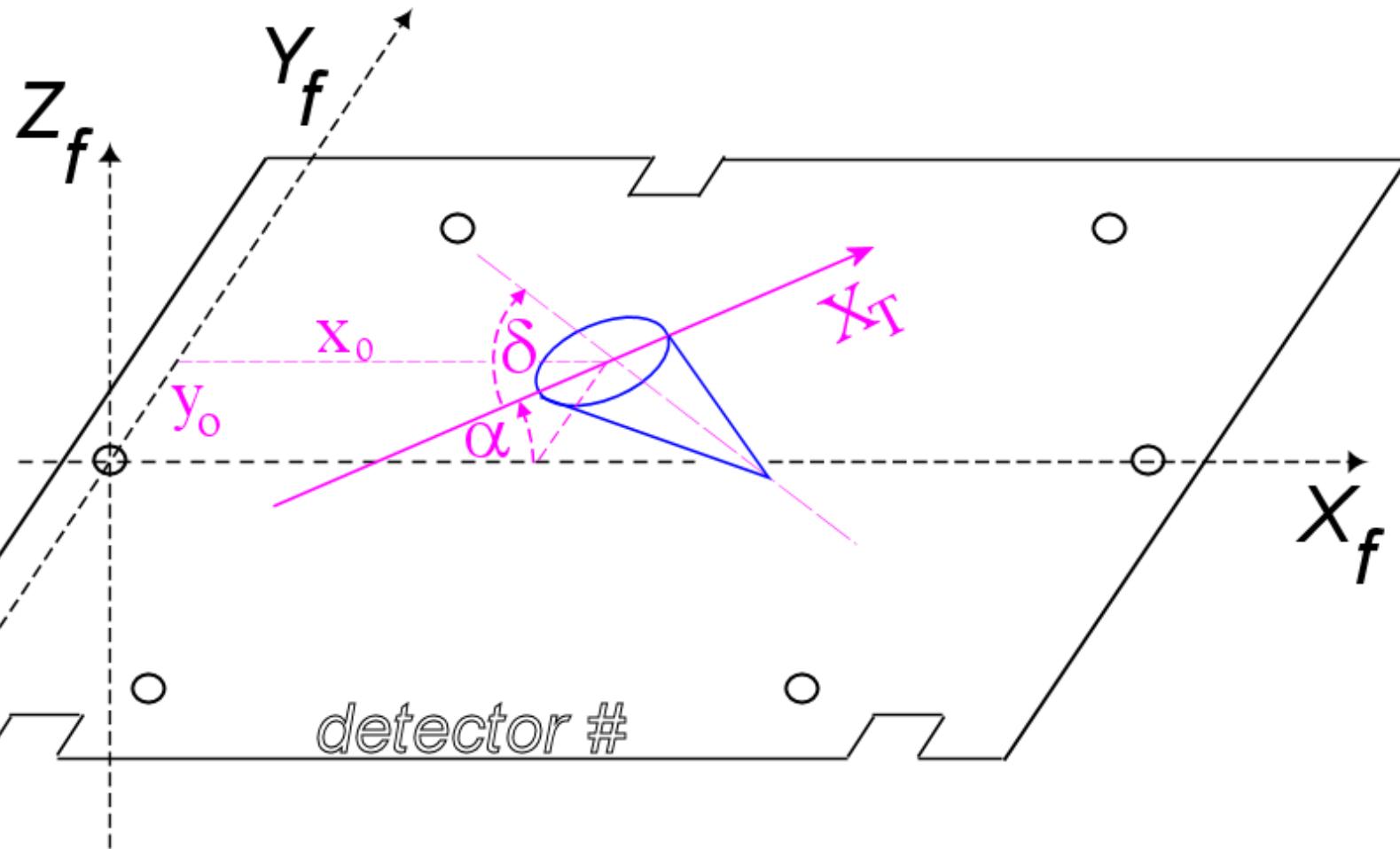
y_S

X_f

X_S

detector #

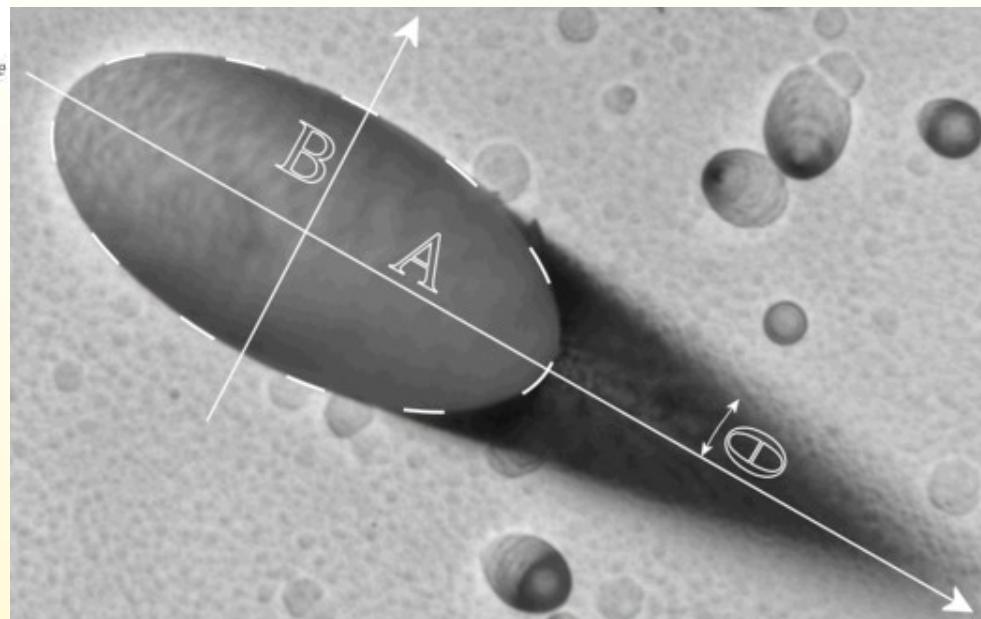
Position and orientation of etch tracks in the detector system



2D

measurement technique

Principle

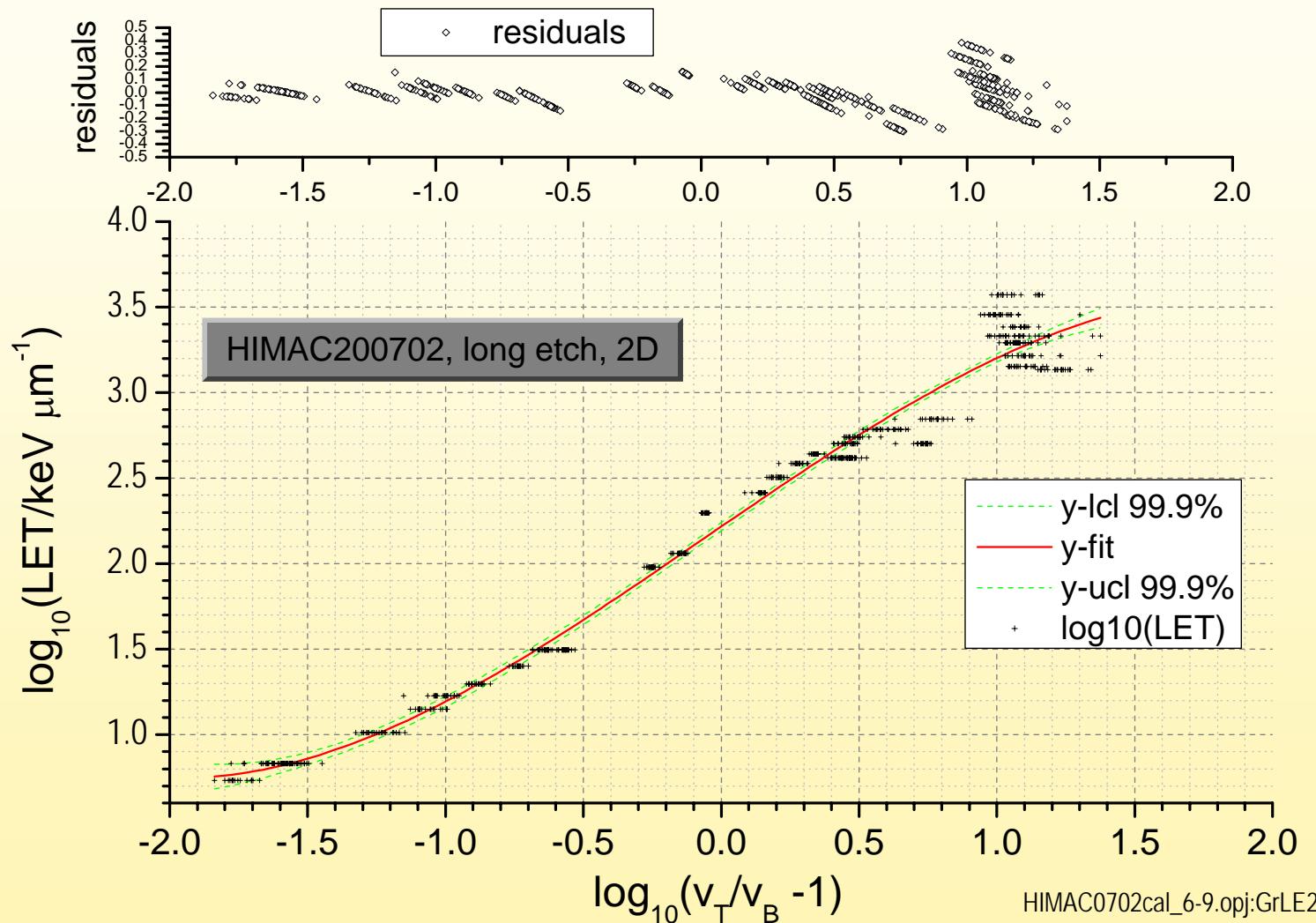


Relative etch rate $R = v_t / v_b = 1 / \sin\theta$

$$R = \sqrt{ \left(\frac{2A}{H} \right)^2 / [1 - (\frac{B}{H})^2]^2 + 1 }$$

A, B: semi- major, minor ellipse axis

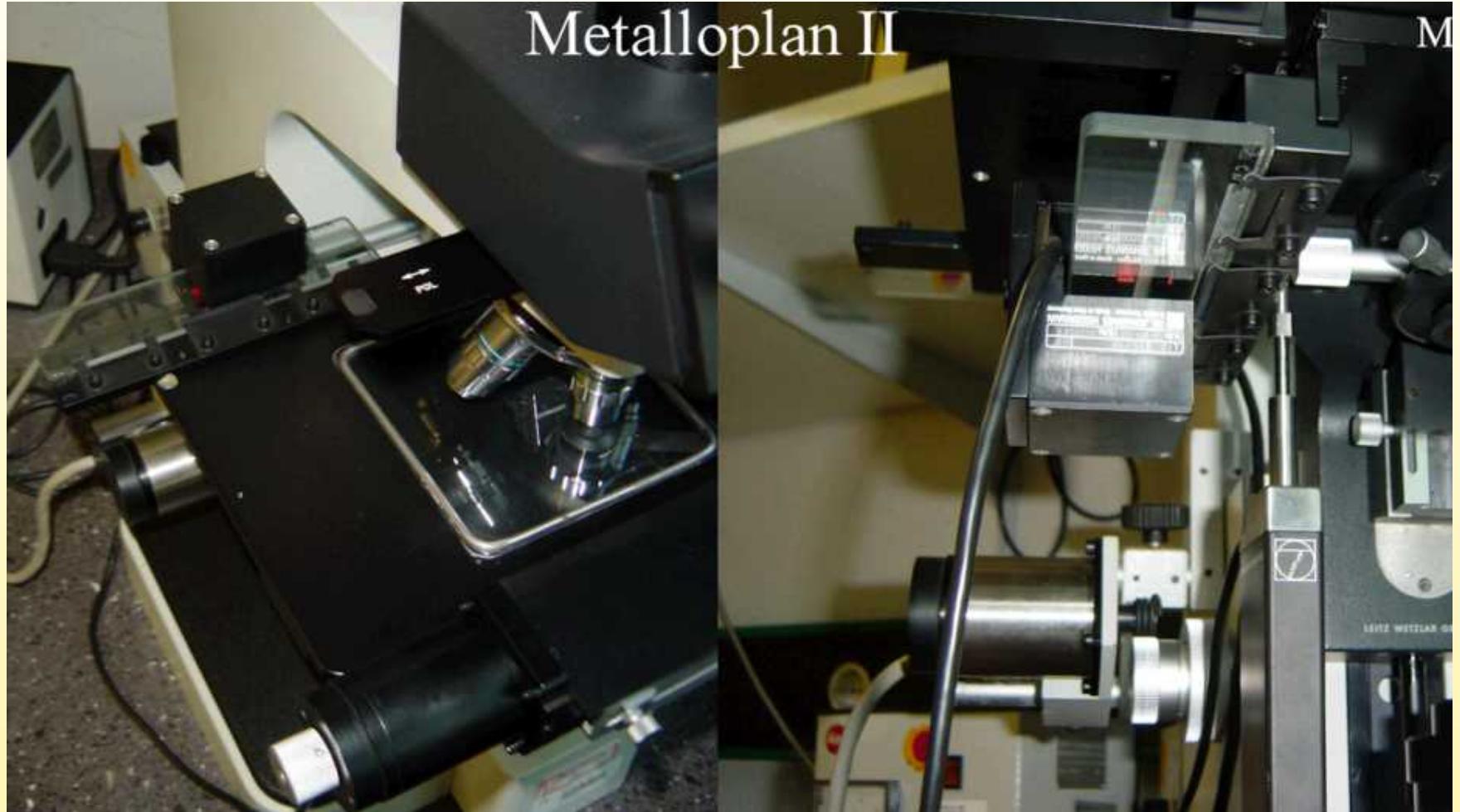
H: bulk etch layer = const. **in space and time !**



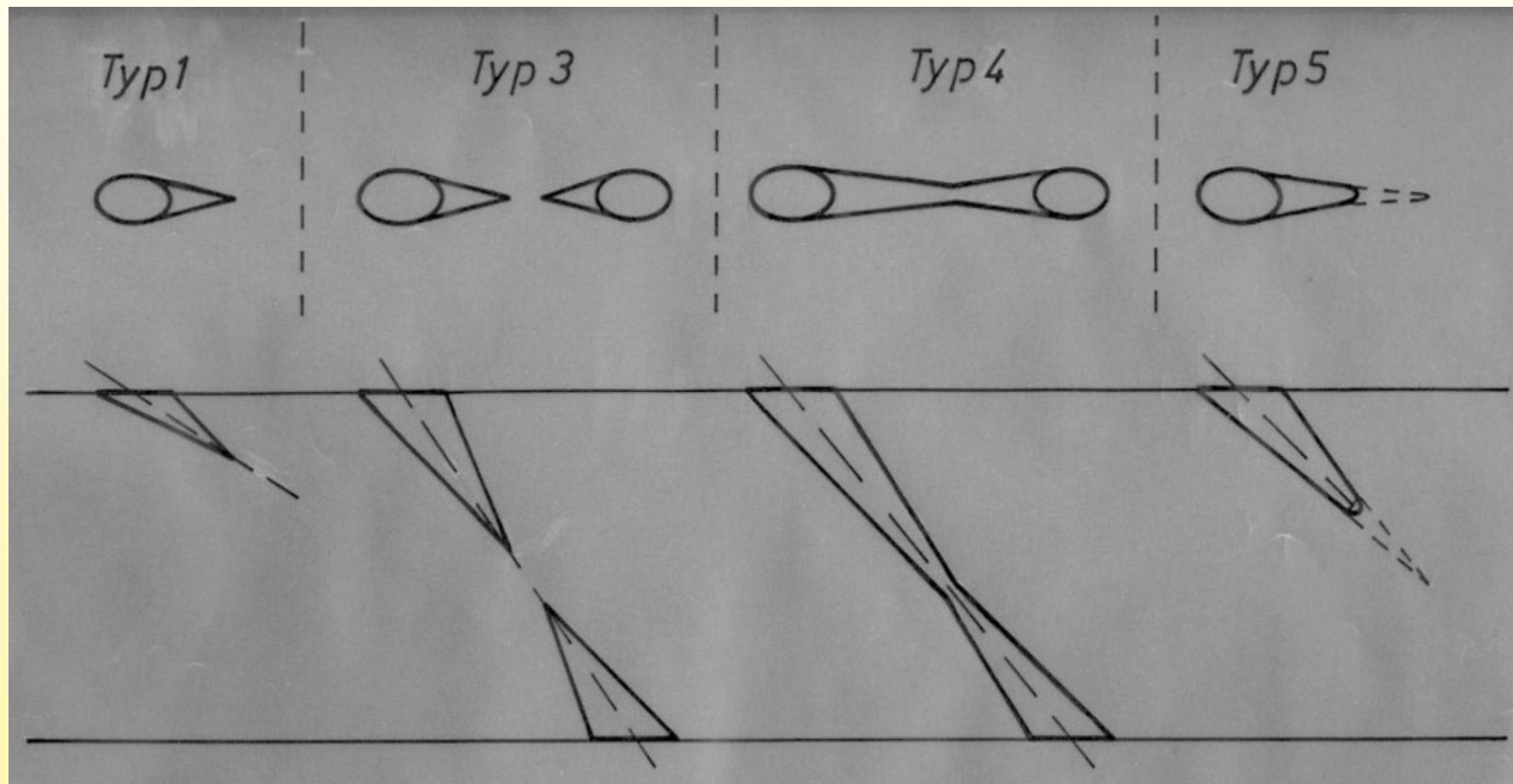
HIMAC0702cal_6-9.opj:GrLE2D

3D measurement technique experimental

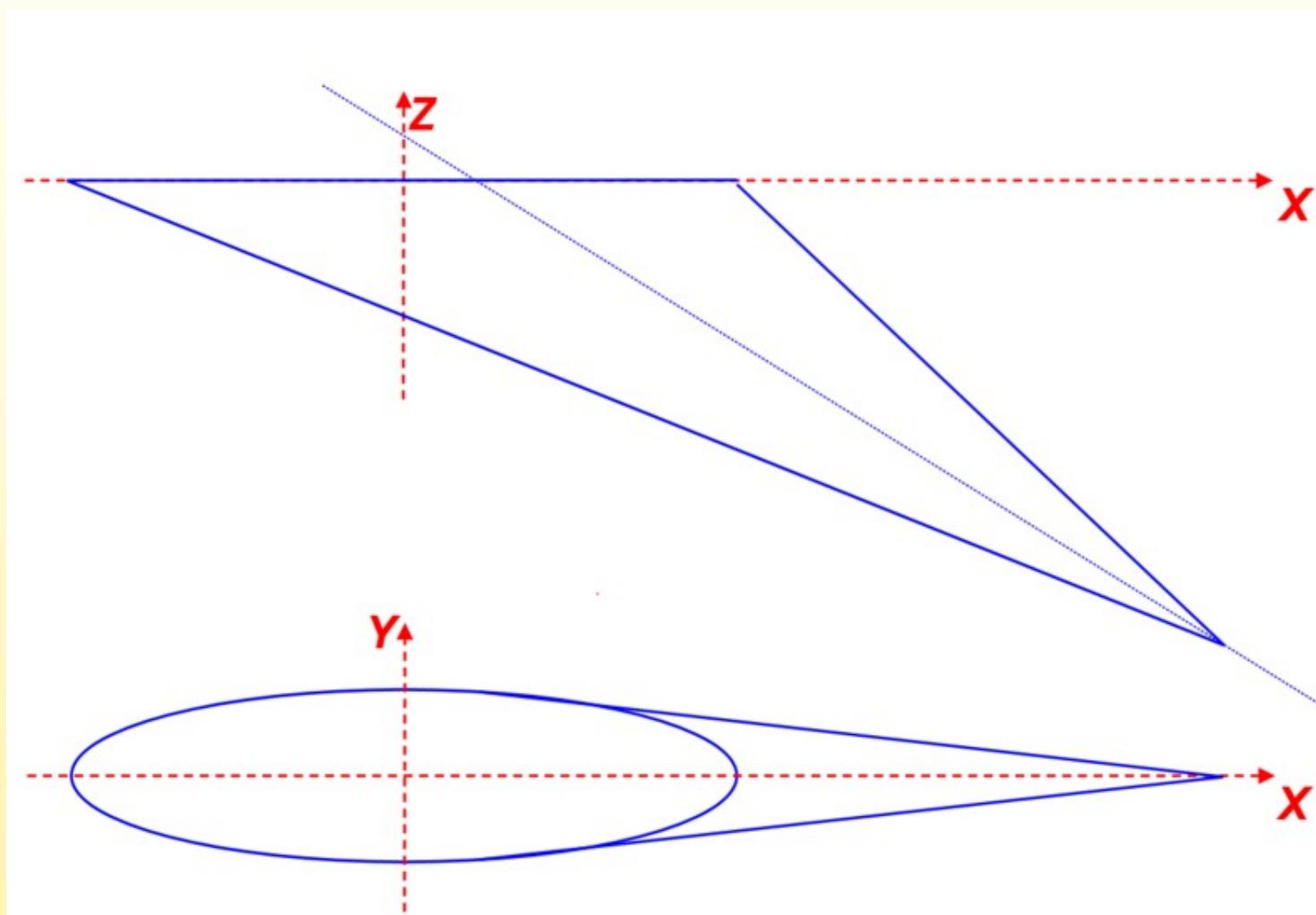
Microscope stage with linear position encoders on three axes (0.1 μm)



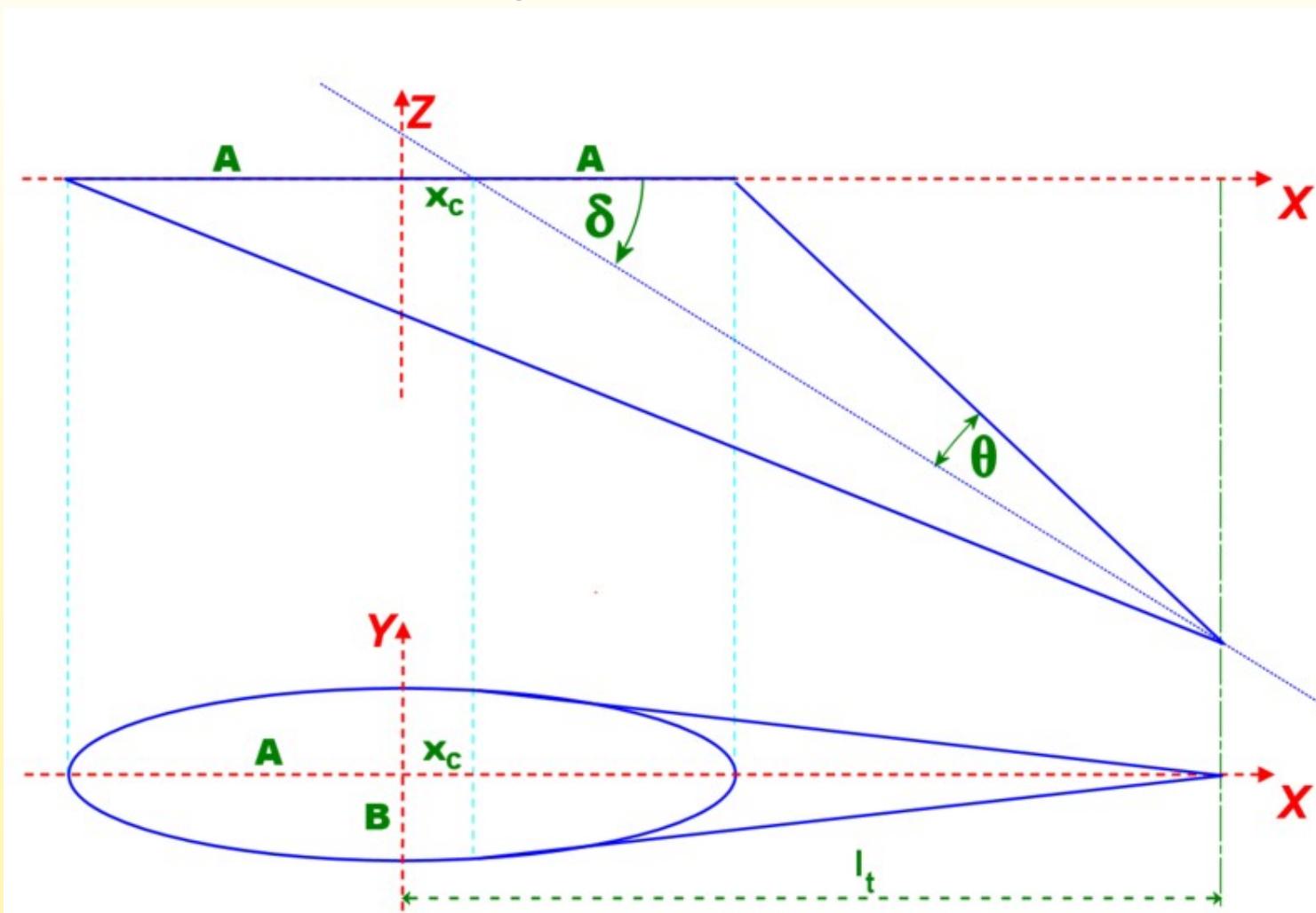
Geometry of etch track types assigned for measurement program



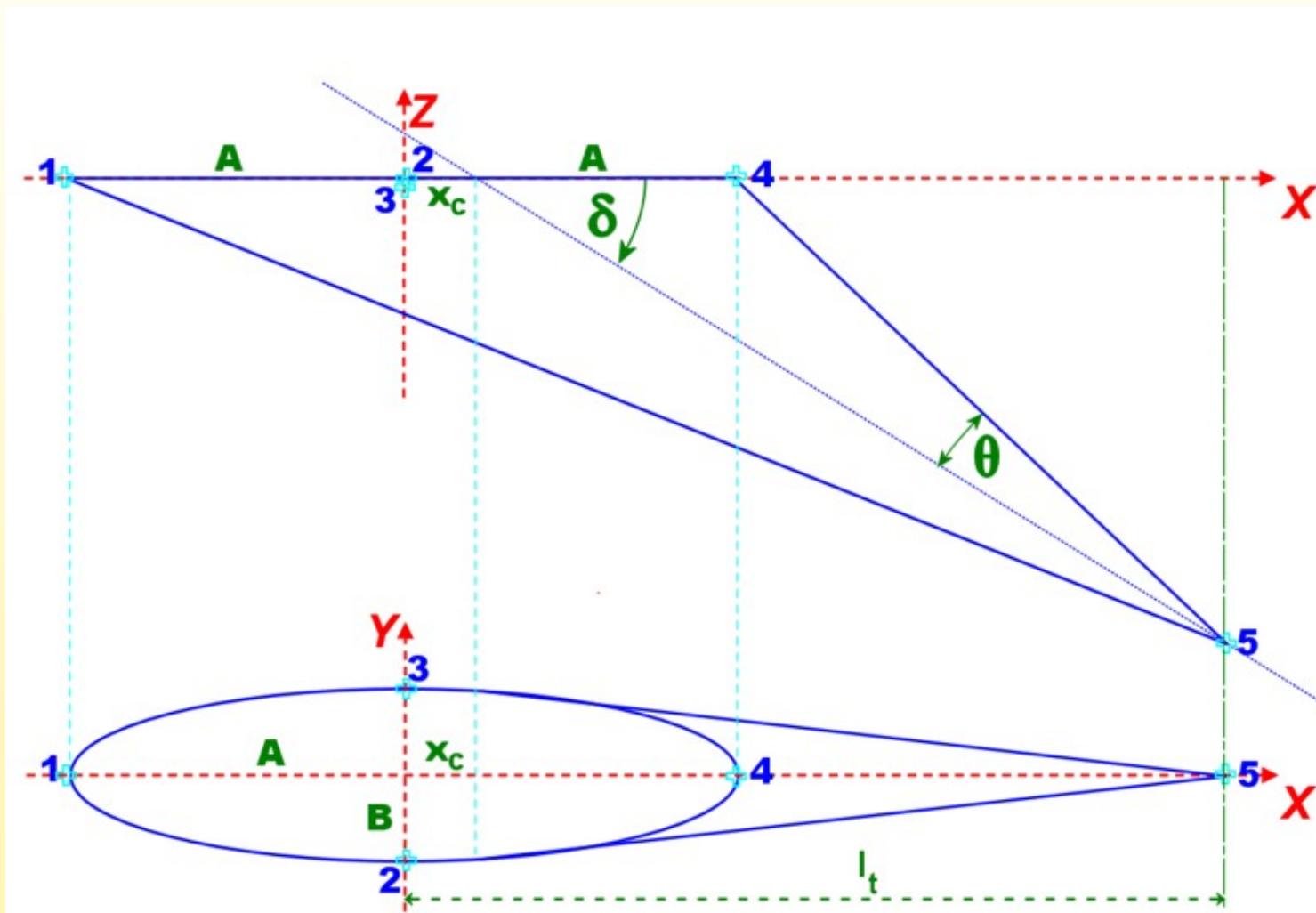
Geometry of etch track type 1 in the track system, T



Parameters defining the size of etch tracks type 1



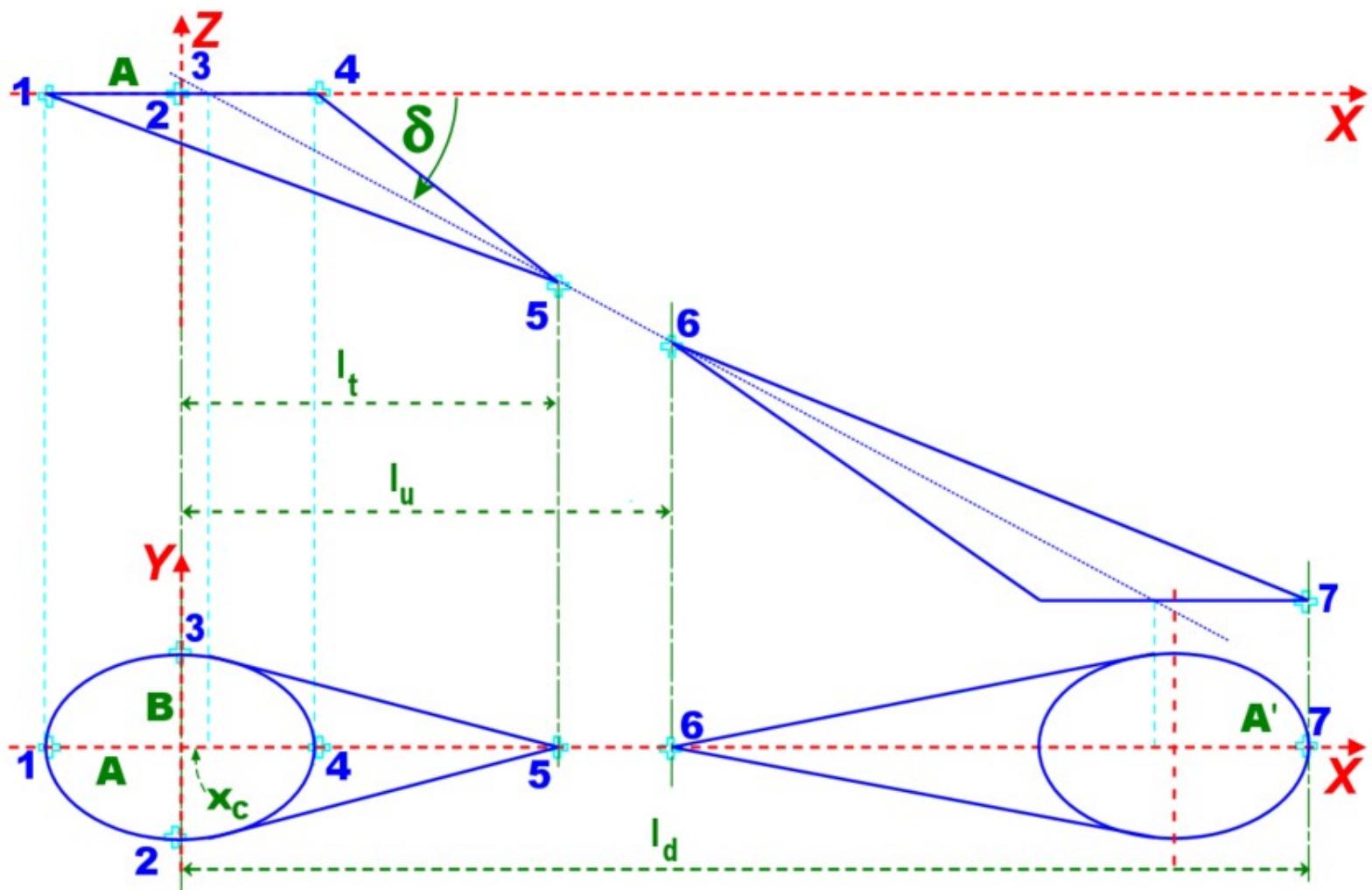
Measurement points for etch tracks type 1



Co-ordinates in the track system, T, of track measuring points for type 1 tracks

Point No.	$X_{T,i}$	$Y_{T,i}$	$Z_{T,i}$
1	-A	0	0
2	0	-B	0
3	0	+B	0
4	+A	0	0
5	l_t	0	$-(l_t - x_c) * \operatorname{tg}(\delta)$

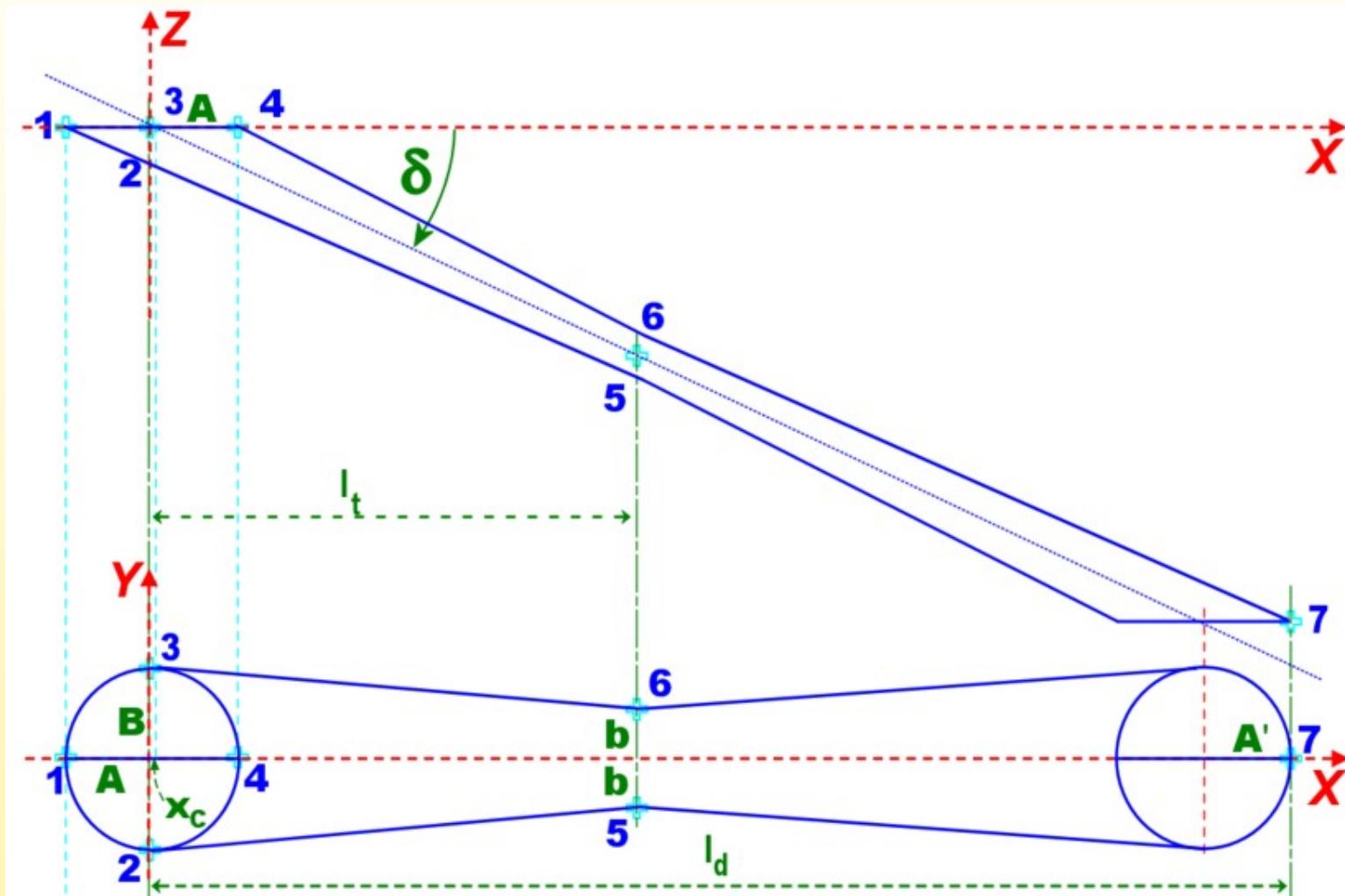
Measurement points for etch tracks type 3



Co-ordinates in the track system, T, of track measuring points for type 3 tracks

Point No.	$X_{T,i}$	$Y_{T,i}$	$Z_{T,i}$
1	-A	0	0
2	0	-B	0
3	0	+B	0
4	+A	0	0
5	l_t	0	$-(l_t - x_c) * \text{tg}(\delta)$
6	l_u	0	$-(l_u - x_c) * \text{tg}(\delta)$
7	l_d	0	$-(l_d - A' - 2x_c) * \text{tg}(\delta)$

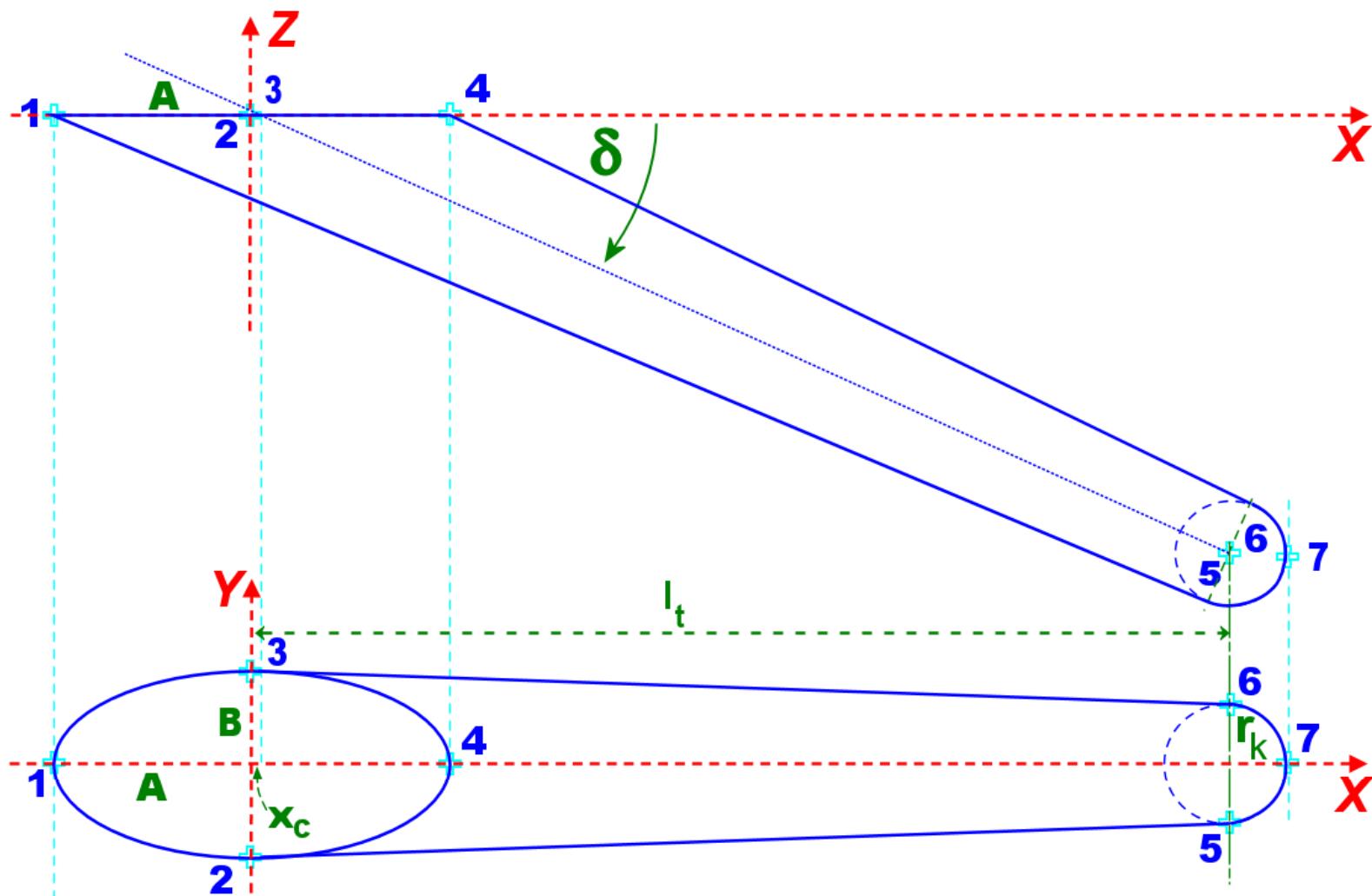
Measurement points for etch tracks type 4



Co-ordinates in the track system, T, of track measuring points for type 4 tracks

Point No.	$X_{T,i}$	$Y_{T,i}$	$Z_{T,i}$
1	-A	0	0
2	0	-B	0
3	0	+B	0
4	+A	0	0
5	l_t	-b	$-(l_t - x_c) * \text{tg}(\delta)$
6	l_t	+b	$-(l_t - x_c) * \text{tg}(\delta)$
7	l_d	0	$-(l_d - A' - 2x_c) * \text{tg}(\delta)$

Measurement points for etch tracks type 5



Co-ordinates in the track system, T, of track measuring points for type 5 tracks

Point No.	$X_{T,i}$	$Y_{T,i}$	$Z_{T,i}$
1	$-A$	0	0
2	0	$-B$	0
3	0	$+B$	0
4	$+A$	0	0
5	l_t	$-r_k$	$-(l_t - x_c) * \operatorname{tg}(\delta)$
6	l_t	$+r_k$	$-(l_t - x_c) * \operatorname{tg}(\delta)$
7	$l_t + r_k$	0	$-(l_t - x_c) * \operatorname{tg}(\delta)$

3D measurement technique theoretical analysis

Transformation of co-ordinates from the track system, T, into the detector system, F.

$$\begin{aligned}X_{F,i} &= X_{T,i} \cos(\alpha) - Y_{T,i} \sin(\alpha) + X_0 \\Y_{F,i} &= X_{T,i} \sin(\alpha) + Y_{T,i} \cos(\alpha) + Y_0 \\Z_{F,i} &= Z_{T,i} + Z_0\end{aligned}$$

Co-ordinates in detector system, F, of track measuring points for type 1 tracks

Point No.	$X_{F,i}$	$Y_{F,i}$	$Z_{F,i}$
1	$x_0 - A \cdot \cos(\alpha)$	$y_0 - A \cdot \sin(\alpha)$	z_0
2	$x_0 + B \cdot \sin(\alpha)$	$y_0 - B \cdot \cos(\alpha)$	z_0
3	$x_0 - B \cdot \sin(\alpha)$	$y_0 + B \cdot \cos(\alpha)$	z_0
4	$x_0 + A \cdot \cos(\alpha)$	$y_0 + A \cdot \sin(\alpha)$	z_0
5	$x_0 + l_t \cdot \cos(\alpha)$	$y_0 + l_t \cdot \sin(\alpha)$	$z_0 - (l_t - x_c) \cdot \tan(\delta)$

Free parameters for track type 1:

$x_0, y_0, z_0, \alpha; A, B, \delta, x_c; l_t$

Co-ordinates in detector system, F, of track measuring points for type 3 tracks

Point No.	$X_{F,i}$	$Y_{F,i}$	$Z_{F,i}$
1	$x_0 - A \cdot \cos(\alpha)$	$y_0 - A \cdot \sin(\alpha)$	z_0
2	$x_0 + B \cdot \sin(\alpha)$	$y_0 - B \cdot \cos(\alpha)$	z_0
3	$x_0 - B \cdot \sin(\alpha)$	$y_0 + B \cdot \cos(\alpha)$	z_0
4	$x_0 + A \cdot \cos(\alpha)$	$y_0 + A \cdot \sin(\alpha)$	z_0
5	$x_0 + l_t \cdot \cos(\alpha)$	$y_0 + l_t \cdot \sin(\alpha)$	$z_0 - (l_t - x_c) \cdot \operatorname{tg}(\delta)$
6	$x_0 + l_u \cdot \cos(\alpha)$	$y_0 + l_u \cdot \sin(\alpha)$	$z_0 - (l_u - x_c) \cdot \operatorname{tg}(\delta)$
7	$x_0 + l_d \cdot \cos(\alpha)$	$y_0 + l_d \cdot \sin(\alpha)$	$z_0 - (l_d - A' - 2x_c) \cdot \operatorname{tg}(\delta)$

Free parameters for track type 3:

$x_0, y_0, z_0, \alpha; A, B, \delta, x_c; l_t, l_u, l_d, A'$

Co-ordinates in detector system, F, of track measuring points for type 4 tracks

Point No.	$X_{F,i}$	$Y_{F,i}$	$Z_{F,i}$
1	$x_0 - A \cdot \cos(\alpha)$	$y_0 - A \cdot \sin(\alpha)$	z_0
2	$x_0 + B \cdot \sin(\alpha)$	$y_0 - B \cdot \cos(\alpha)$	z_0
3	$x_0 - B \cdot \sin(\alpha)$	$y_0 + B \cdot \cos(\alpha)$	z_0
4	$x_0 + A \cdot \cos(\alpha)$	$y_0 + A \cdot \sin(\alpha)$	z_0
5	$x_0 + l_t \cdot \cos(\alpha) + b \cdot \sin(\alpha)$	$y_0 + l_t \cdot \sin(\alpha) - b \cdot \cos(\alpha)$	$z_0 - (l_t - x_c) \cdot \operatorname{tg}(\delta)$
6	$x_0 + l_t \cdot \cos(\alpha) - b \cdot \sin(\alpha)$	$y_0 + l_t \cdot \sin(\alpha) + b \cdot \cos(\alpha)$	$z_0 - (l_t - x_c) \cdot \operatorname{tg}(\delta)$
7	$x_0 + l_d \cdot \cos(\alpha)$	$y_0 + l_d \cdot \sin(\alpha)$	$z_0 - (l_d - A' - 2x_c) \cdot \operatorname{tg}(\delta)$

Free parameters for track type 4:

$x_0, y_0, z_0, \alpha; A, B, \delta, x_c; l_t, b, l_d, A'$

Co-ordinates in detector system, F, of track measuring points for type 5 tracks

Point No.	$X_{F,i}$	$Y_{F,i}$	$Z_{F,i}$
1	$x_0 - A \cdot \cos(\alpha)$	$y_0 - A \cdot \sin(\alpha)$	z_0
2	$x_0 + B \cdot \sin(\alpha)$	$y_0 - B \cdot \cos(\alpha)$	z_0
3	$x_0 - B \cdot \sin(\alpha)$	$y_0 + B \cdot \cos(\alpha)$	z_0
4	$x_0 + A \cdot \cos(\alpha)$	$y_0 + A \cdot \sin(\alpha)$	z_0
5	$x_0 + l_t \cdot \cos(\alpha) + r_k \cdot \sin(\alpha)$	$y_0 + l_t \cdot \sin(\alpha) - r_k \cdot \cos(\alpha)$	$z_0 - (l_t - x_c) \cdot \operatorname{tg}(\delta)$
6	$x_0 + l_t \cdot \cos(\alpha) - r_k \cdot \sin(\alpha)$	$y_0 + l_t \cdot \sin(\alpha) + r_k \cdot \cos(\alpha)$	$z_0 - (l_t - x_c) \cdot \operatorname{tg}(\delta)$
7	$x_0 + (l_t + r_k) \cdot \cos(\alpha)$	$y_0 + (l_t + r_k) \cdot \sin(\alpha)$	$z_0 - (l_t - x_c) \cdot \operatorname{tg}(\delta)$

Free parameters for track type 5:

$x_0, y_0, z_0, \alpha; A, B, \delta, x_c; l_t, r_k$

Parameters are sought for the maximum of the likelihood function Λ , resp. its logarithm.

$$\begin{aligned}-2 \cdot \log \Lambda = & \quad n m * \log 2\pi + n k * \log V_{xy} + n(m-k) * \log V_z \\ & + \sum_{a=1}^k (M_{aa} / V_{xy}) + \sum_{a=k+1}^m (M_{aa} / V_z)\end{aligned}$$

$$V_{xy} \cong (1/nk) * \sum_{a=1}^k (M_{aa}); \quad \text{variance of } x,y \text{ measurement}$$

$$V_z \cong (1/n(m-k)) * \sum_{a=k+1}^m (M_{aa}); \quad \text{variance of } z \text{ measurement}$$

“Objective function” $\Psi(\mathbf{M})$ is minimized

$$\Psi(\mathbf{M}) = [nk * \log(\sum_{a=1}^k (M_{aa})) + n(m-k) * \log(\sum_{a=k+1}^m (M_{aa}))] / 2$$

Matrix of moments \mathbf{M}

$$\mathbf{M}(\Theta) = \boldsymbol{\varepsilon} \boldsymbol{\varepsilon}^T$$

vector of residuals/errors $\boldsymbol{\varepsilon}$

$$\boldsymbol{\varepsilon}^T = (X_1(\Theta) - x_1, \dots, X_n(\Theta) - x_n, Y_1(\Theta) - y_1, \dots, Y_n(\Theta) - y_n, Z_1(\Theta) - z_1, \dots, Z_n(\Theta) - z_n)$$

$X_i(\Theta), Y_i(\Theta), Z_i(\Theta)$ = model coordinates

x_i, y_i, z_i = measured coordinates

$i=1 \dots n$

parameter vectors Θ

$$\Theta = (x_0, y_0, z_0, \alpha; A, B, \delta, x_c; I_t); \quad \text{type 1}$$

$$\Theta = (x_0, y_0, z_0, \alpha; A, B, \delta, x_c; I_t, I_u, I_d, A'); \quad \text{type 3}$$

$$\Theta = (x_0, y_0, z_0, \alpha; A, B, \delta, x_c; I_t, b, I_d, A'); \quad \text{type 4}$$

$$\Theta = (x_0, y_0, z_0, \alpha; A, B, \delta, x_c; I_t, r_k); \quad \text{type 5}$$

constraints for parameters

linear:

$$A \geq B > 0; \quad x_c > 0; \quad B > r_k \geq 0 ; \quad B > b \geq 0$$

nonlinear ‘constraint’

$$A/B = \cos\theta / \sqrt{(\cos^2\theta - \cos^2\delta)}$$

leads to the Langrange equation:

$$N_1(A, B, \delta, \theta) = (A^2 - B^2)(1 + \tan^2\delta) - A^2(1 + \tan^2\theta) = 0$$

Determination of cone angle, θ , from track parameters

$$\begin{aligned} \operatorname{tg}(\theta) = & \left\{ \sqrt{[B^2(l_t - w)^2 - (A^2 - B^2)(B^2 - w^2)]} - w^2(l_t - w) \right\} / \\ & / [(l_t - w)^2 - (A^2 - B^2)] * \sqrt{(1 - B^2/A^2)} \end{aligned}$$

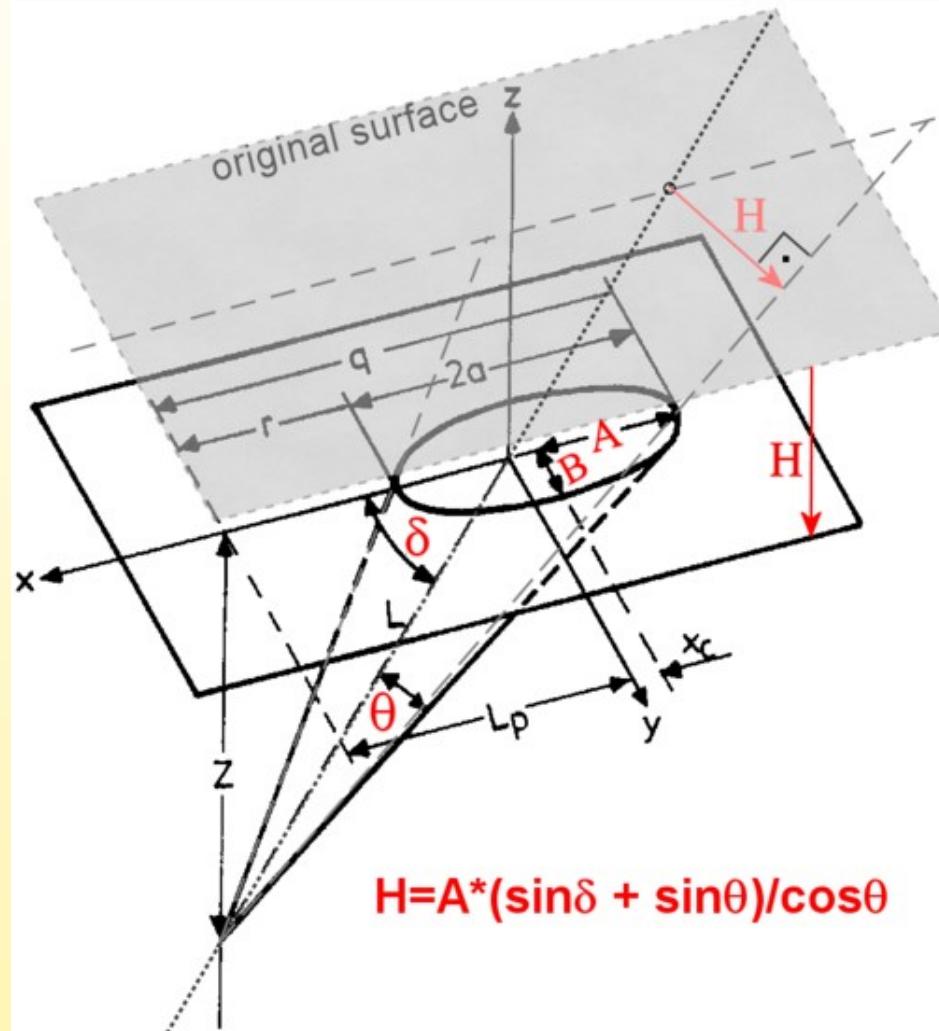
$$\theta > 0$$

w = b for type 4; w = r_k for type 5; w=0 otherwise

Determination of local bulk layer, H, from track parameters

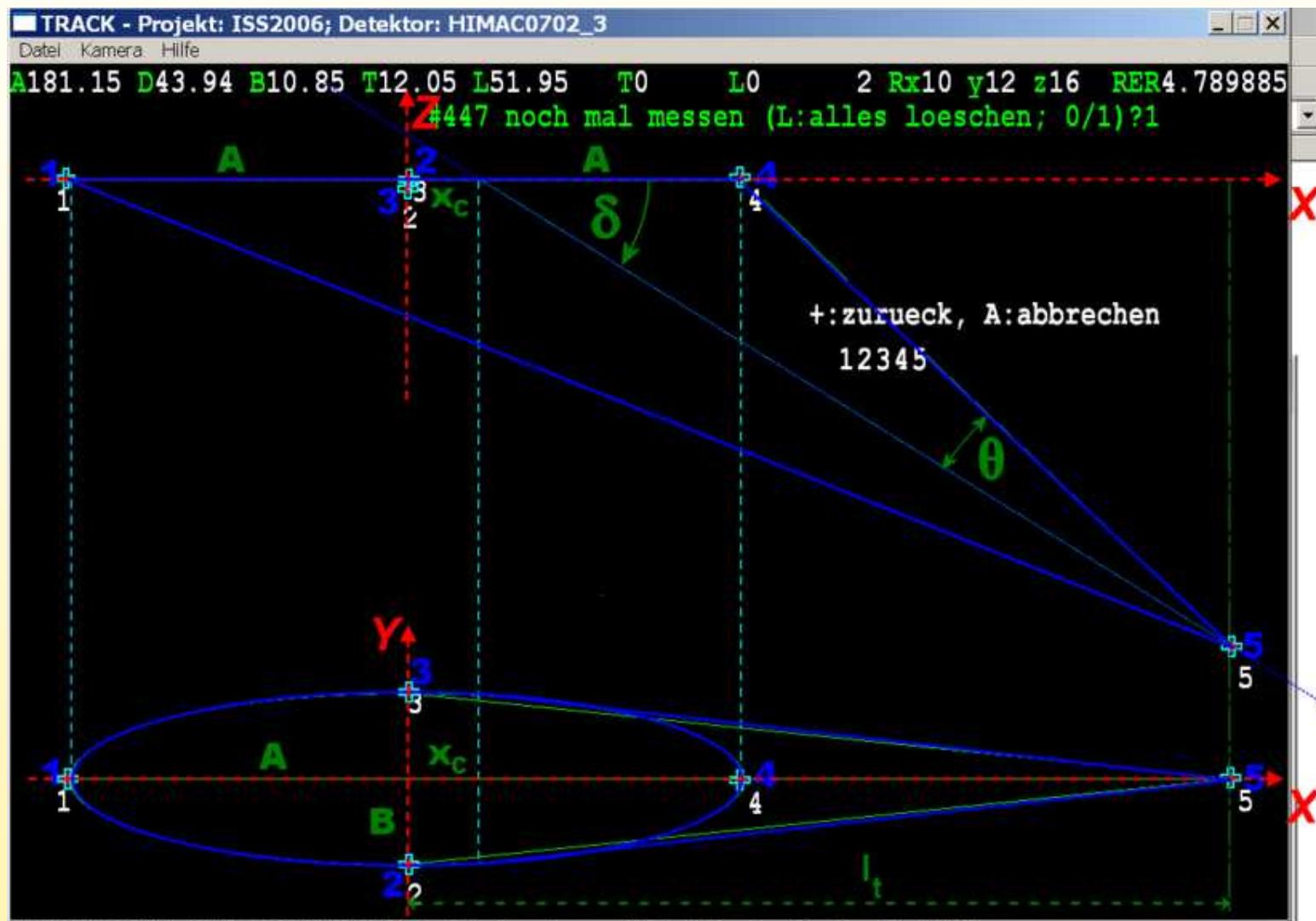
$$H = A * (\sin\delta + \sin\theta) / \cos\theta$$

Ideal etch cone relations

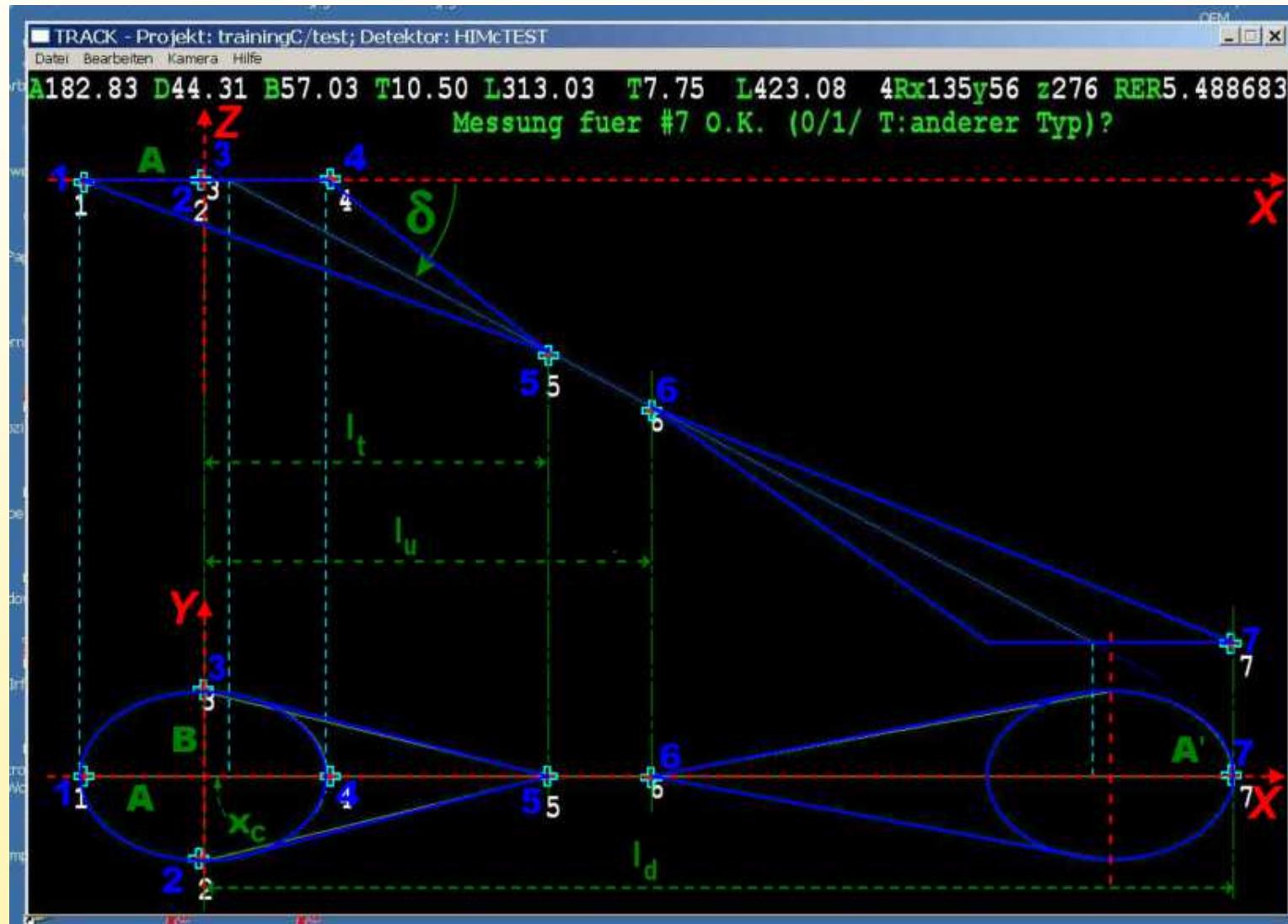


3D measurements – accuracy/precision

Screen shot of type 1 measurement with schematic

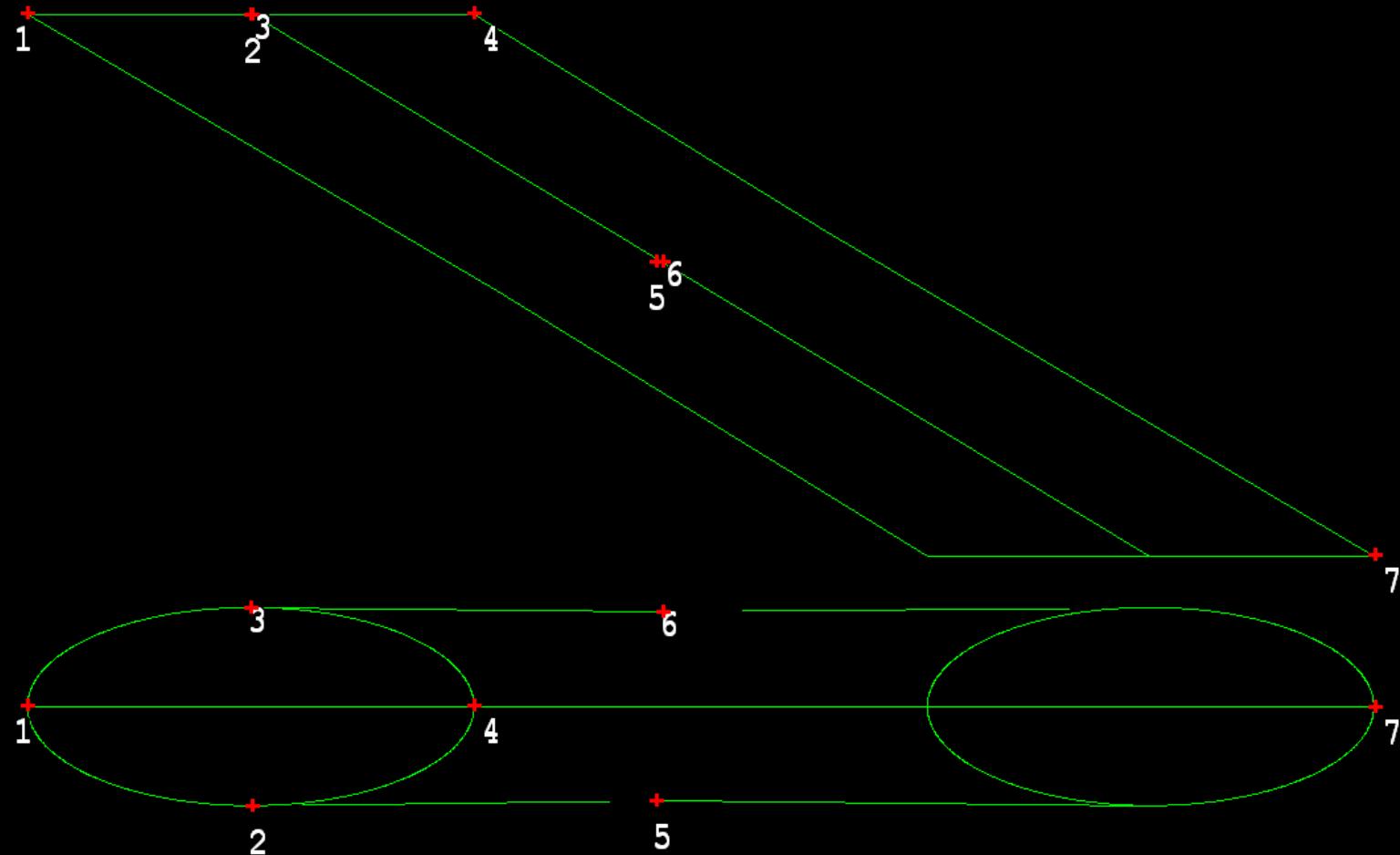


Screen shot of type 3 measurement with schematic

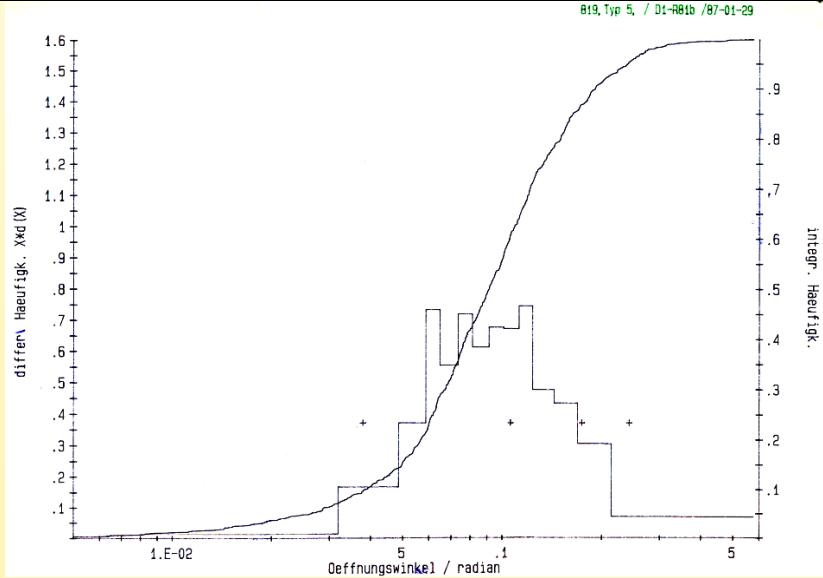
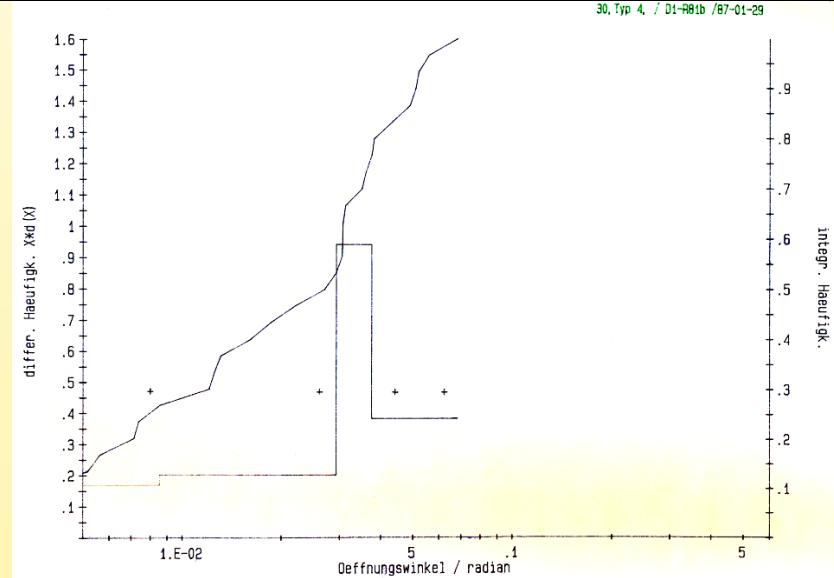
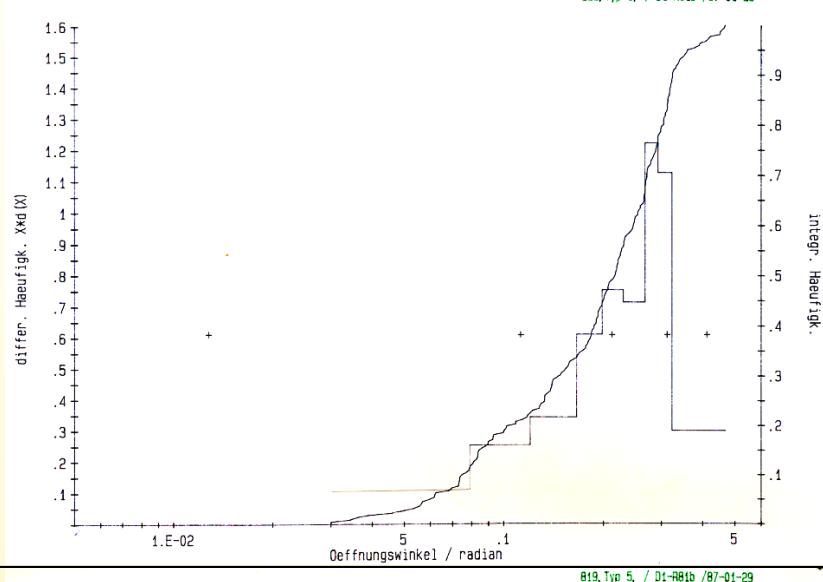
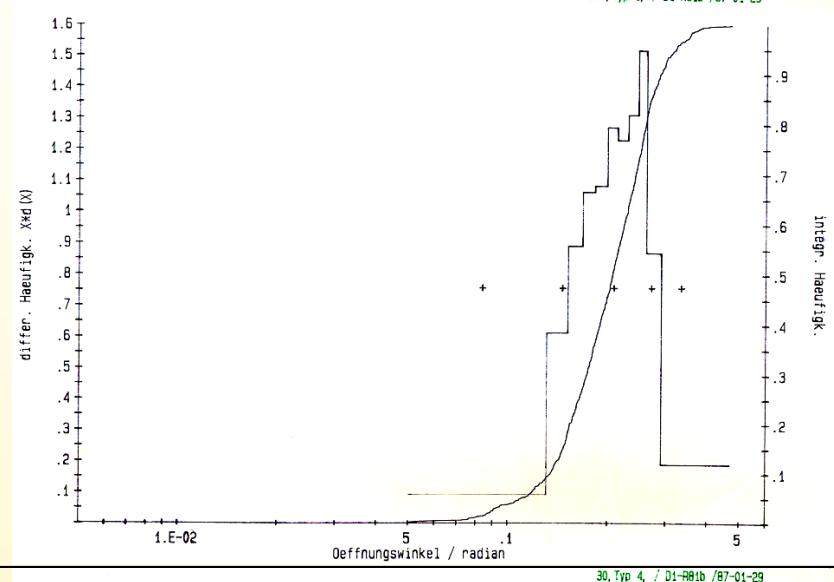


Screen shot of type 4 measurement

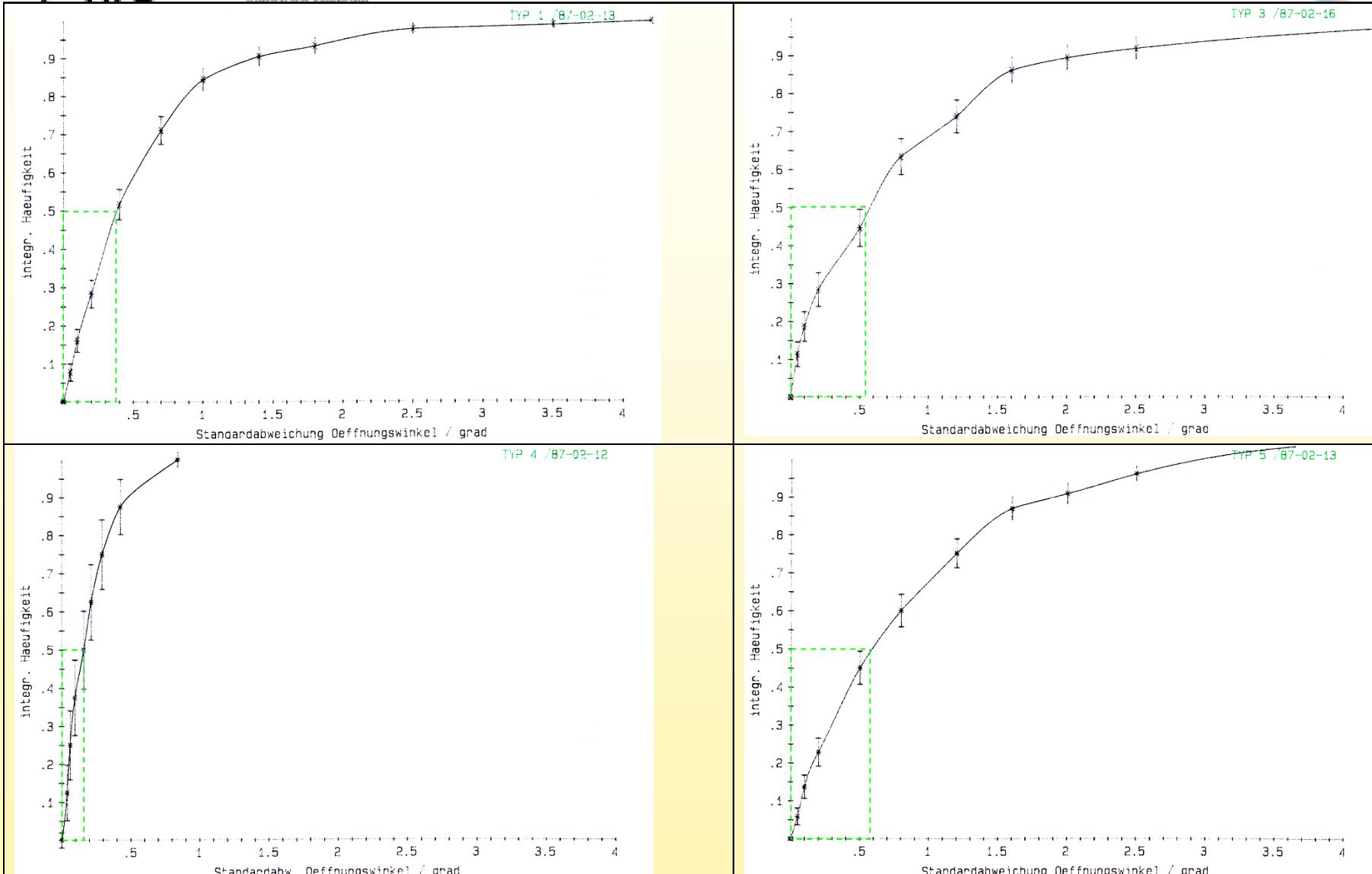
A0.21 D61.45 B52.95 T0.57 L288.94 T0.48 L344.35 3Rx58 y38 z42 RER100.0660
48 Messung fuer #370 O.K. (0/1/ T:anderer Typ)?



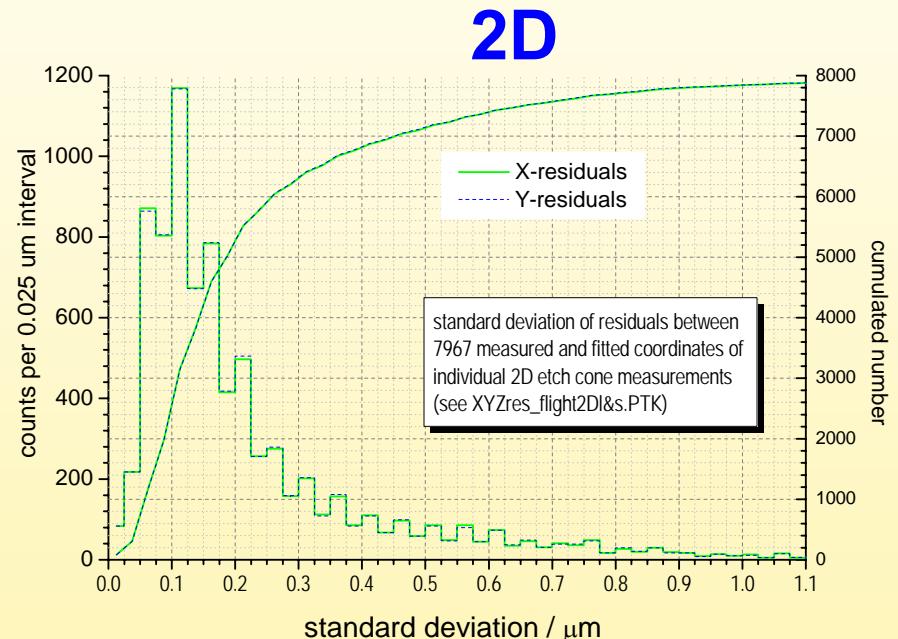
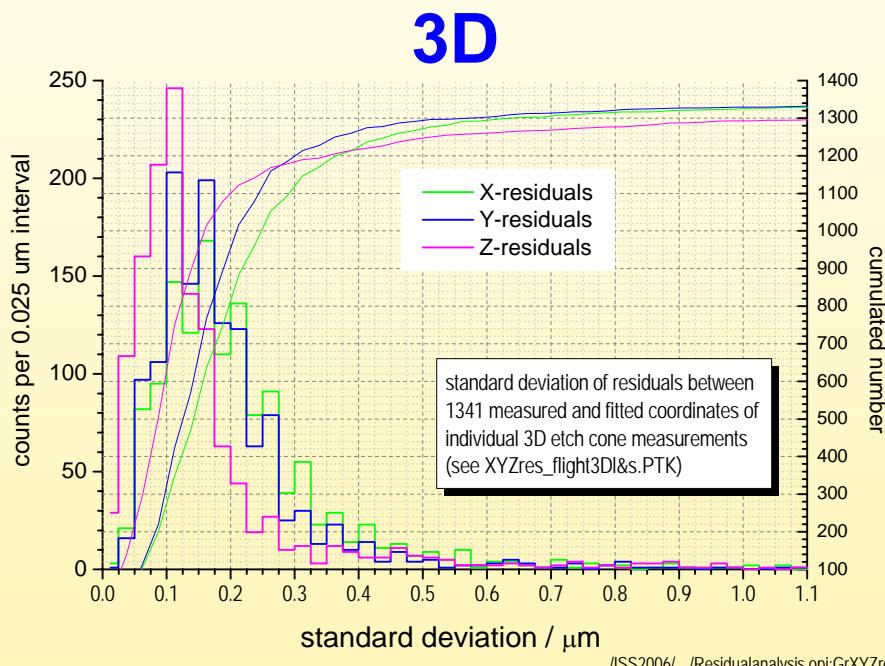
Distributions of cone angle measurements (cellulose nitrate)



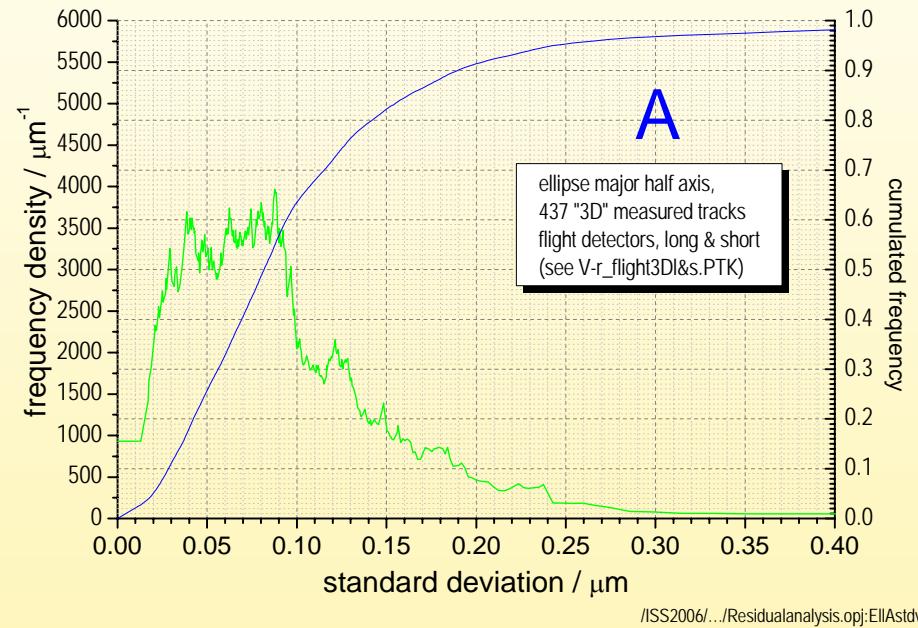
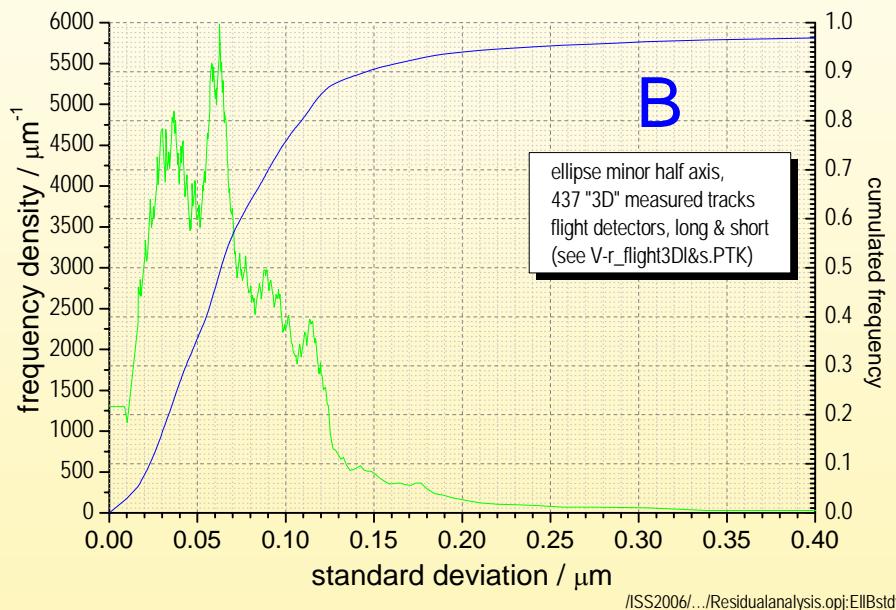
Distributions of cone angle measurement errors (CN)



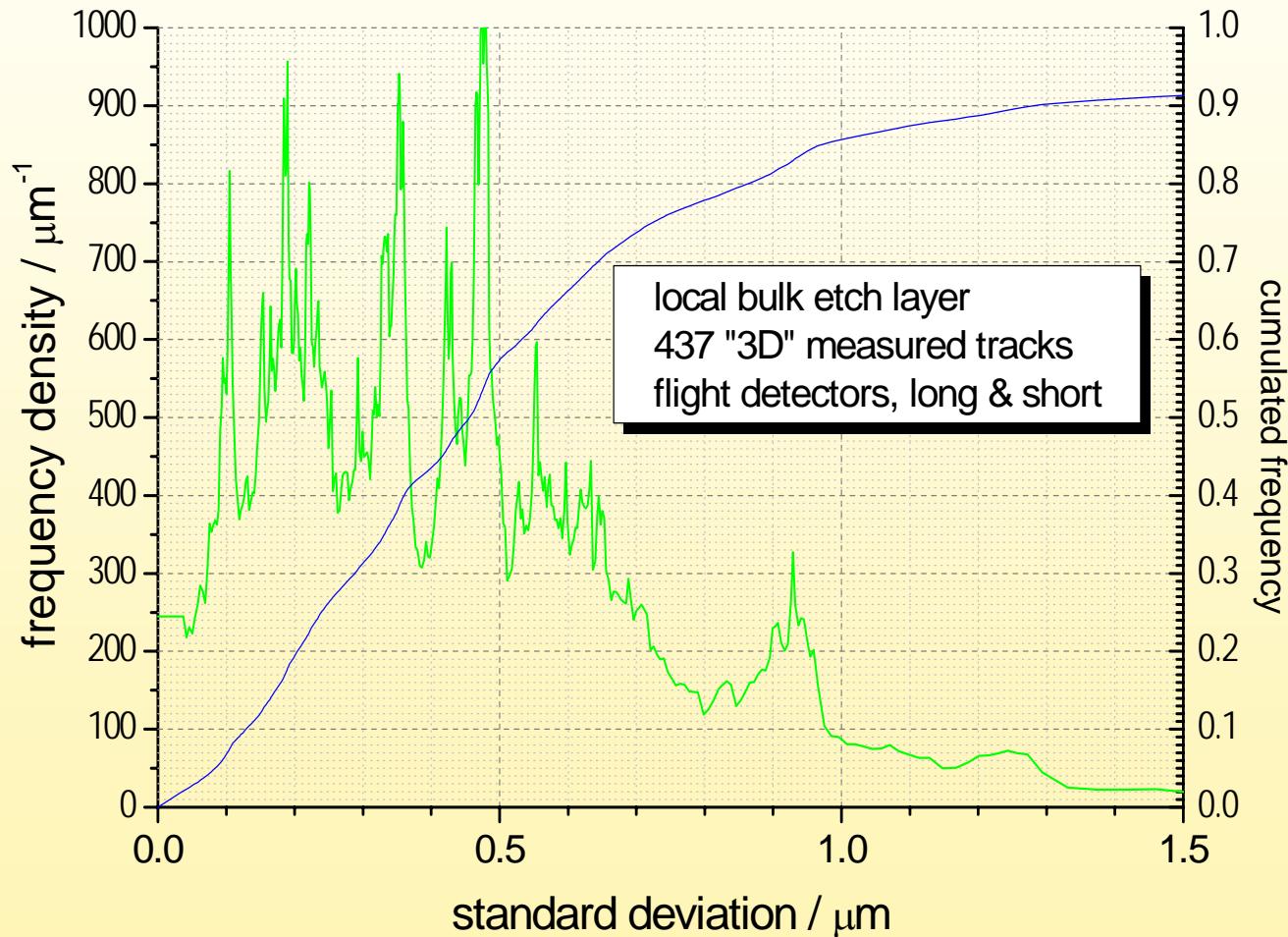
Precision of co-ordinate measurements; 3D vs. 2D (CR 39, standard deviation of residuals)



Precision of ellipse semi axes - 3D (CR 39, standard deviation of repetitions)



Precision of local bulk layer measurements - 3D (CR 39, standard deviation of repetitions)



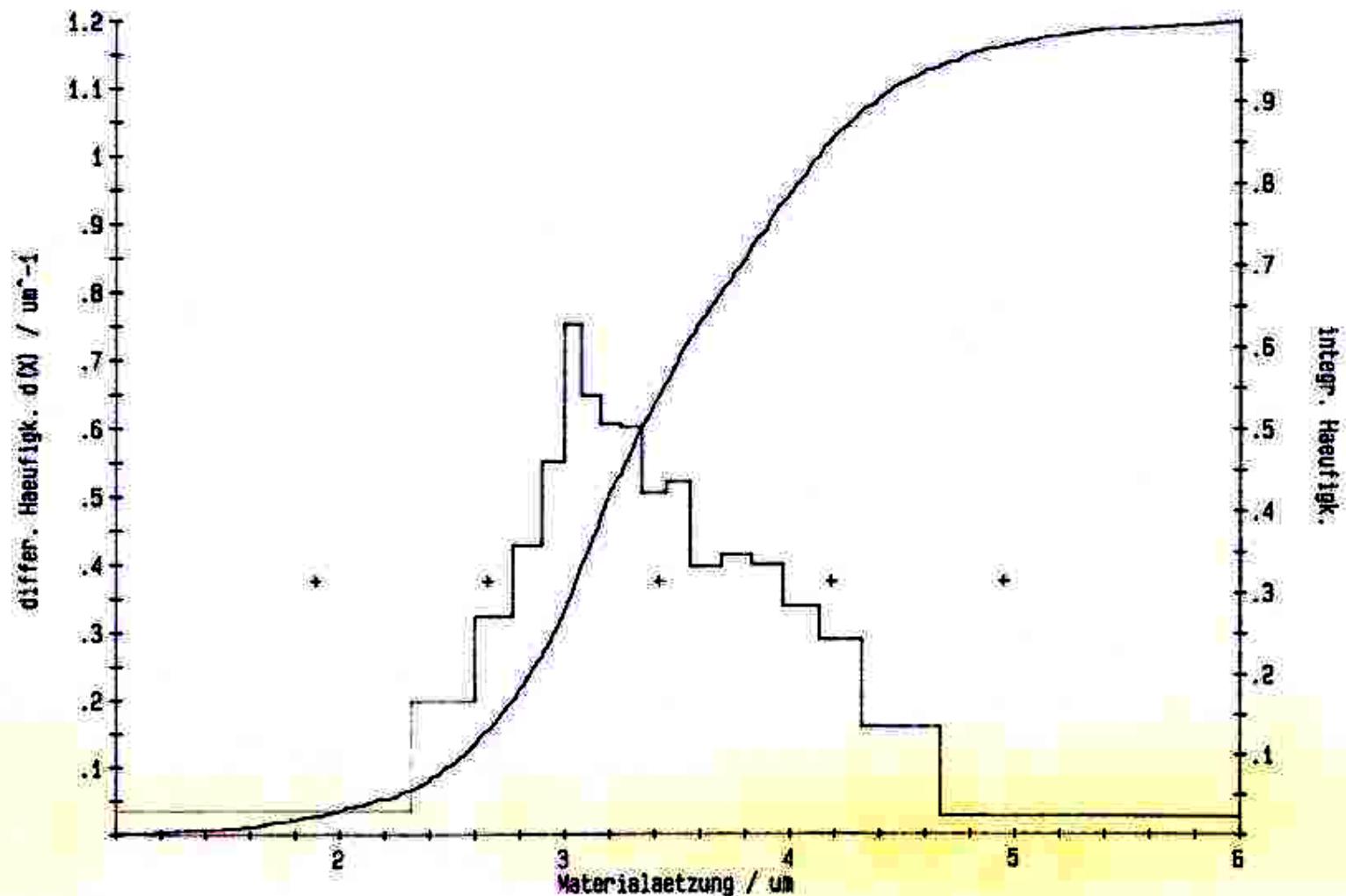
/ISS2006/..../Residualanalysis.opj:Bulkstdv

local bulk layer data

(cellulose nitrate, D1 mission)

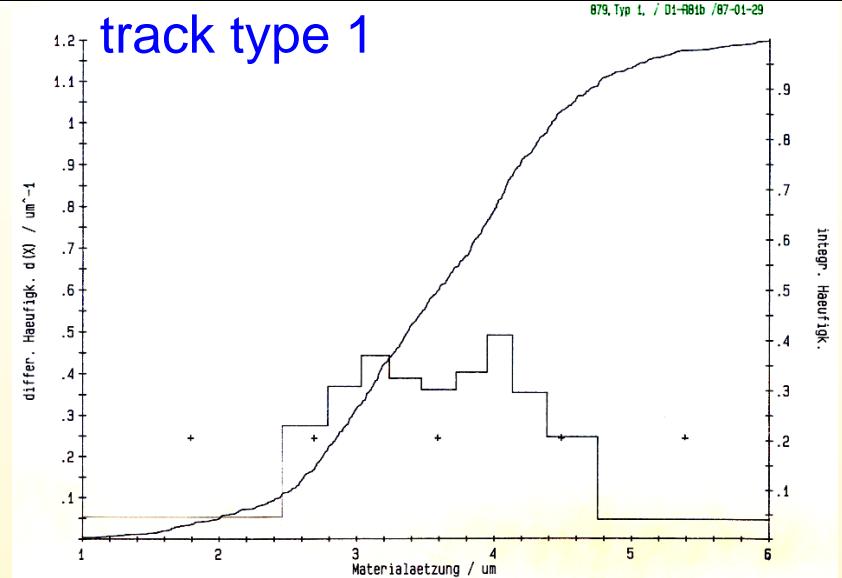
Distribution of local bulk layer measurements (cellulose nitrate)

1950 alle. / D1-R31b / 07-01-29

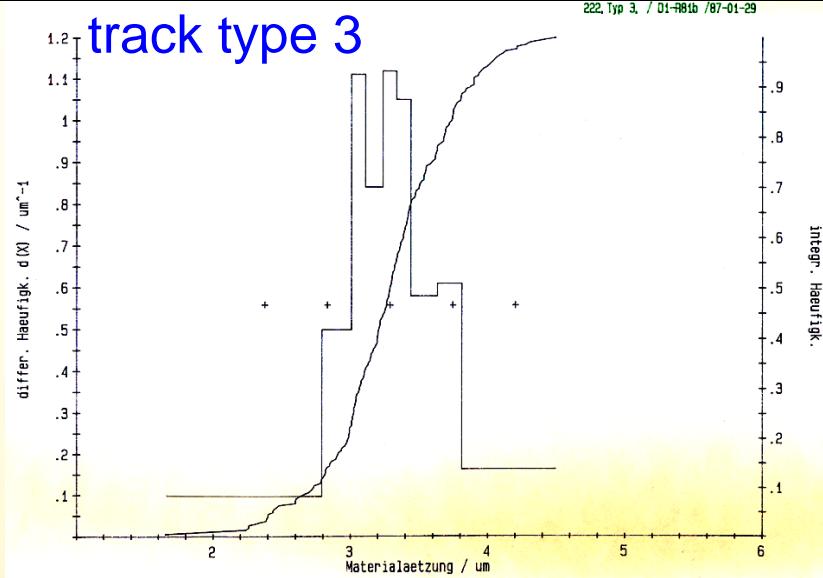


Distributions of local bulk layer measurements (CN)

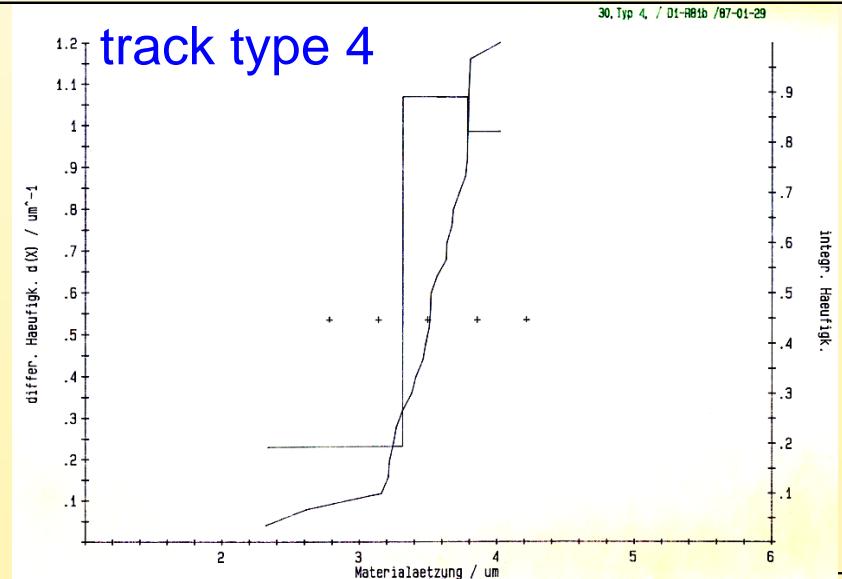
track type 1



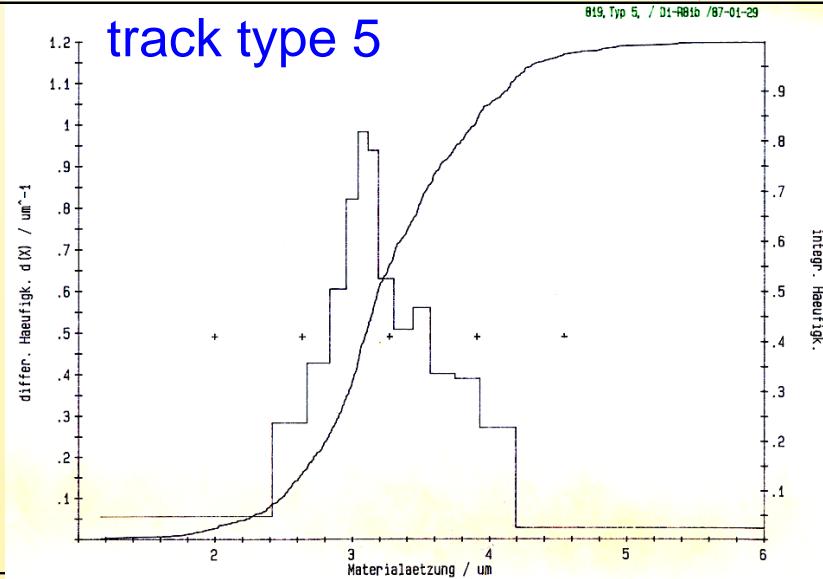
track type 3



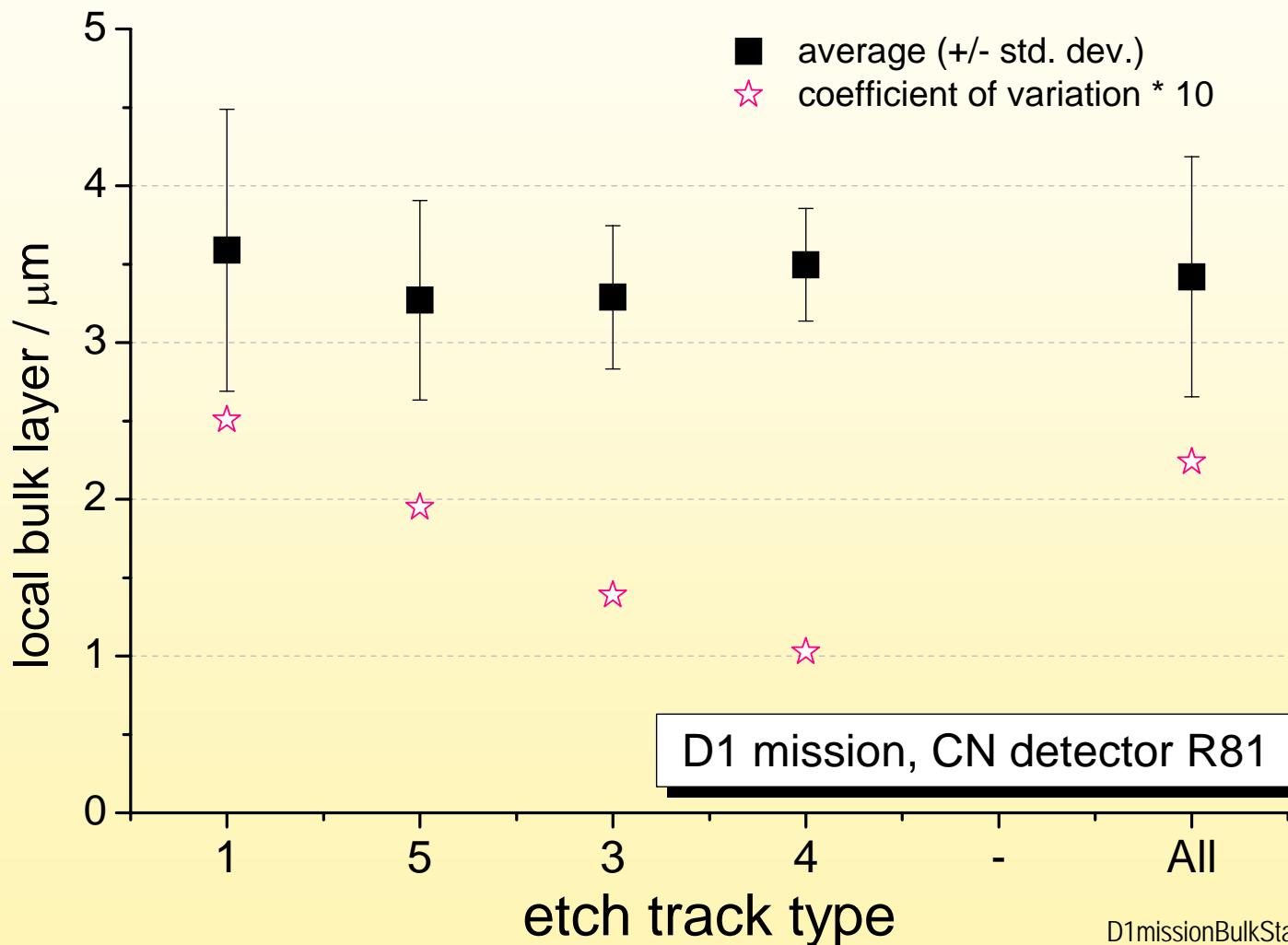
track type 4



track type 5



Summary of local bulk layer measurements (CN)

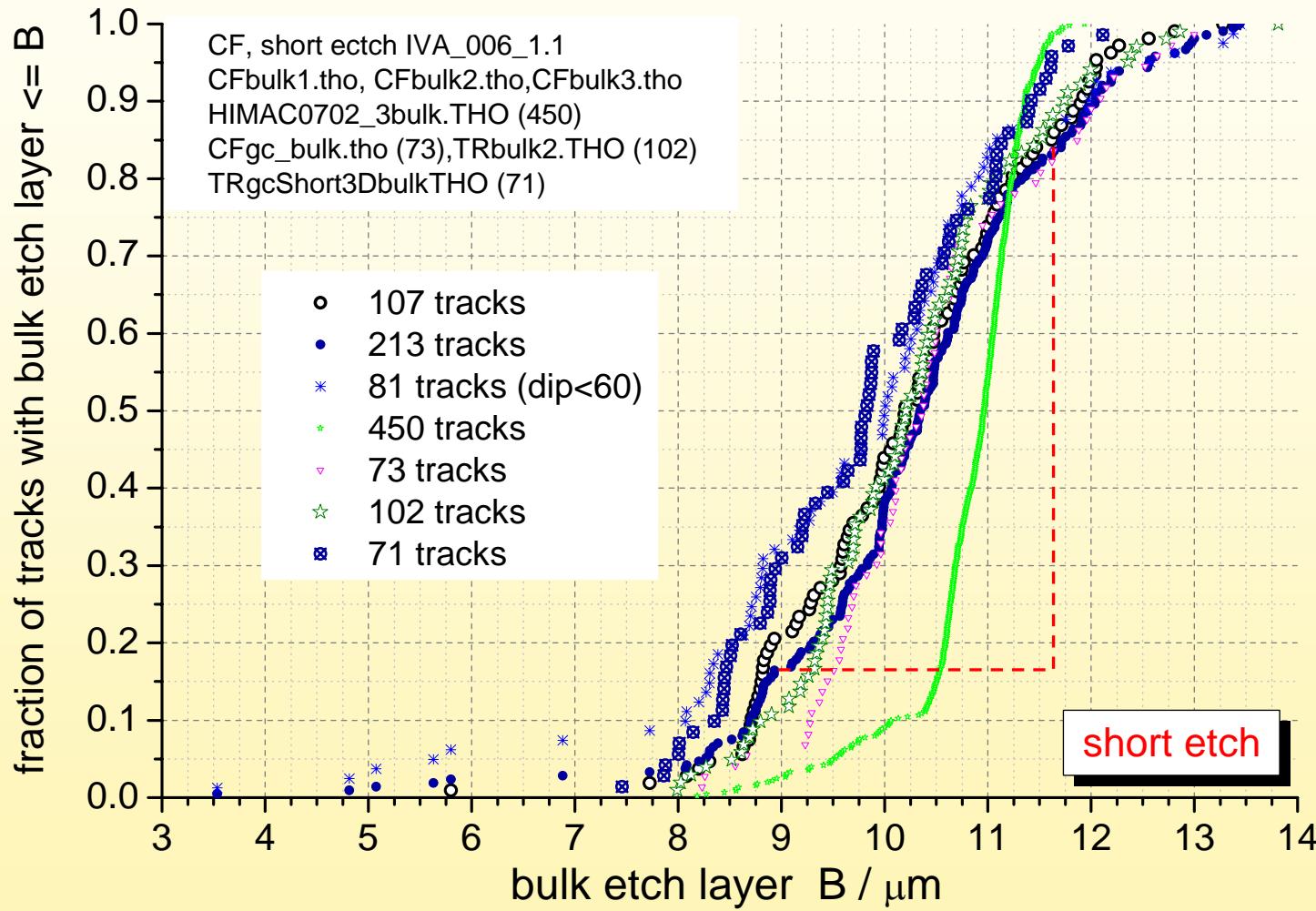


D1missionBulkStatistics.opj

local bulk layer data

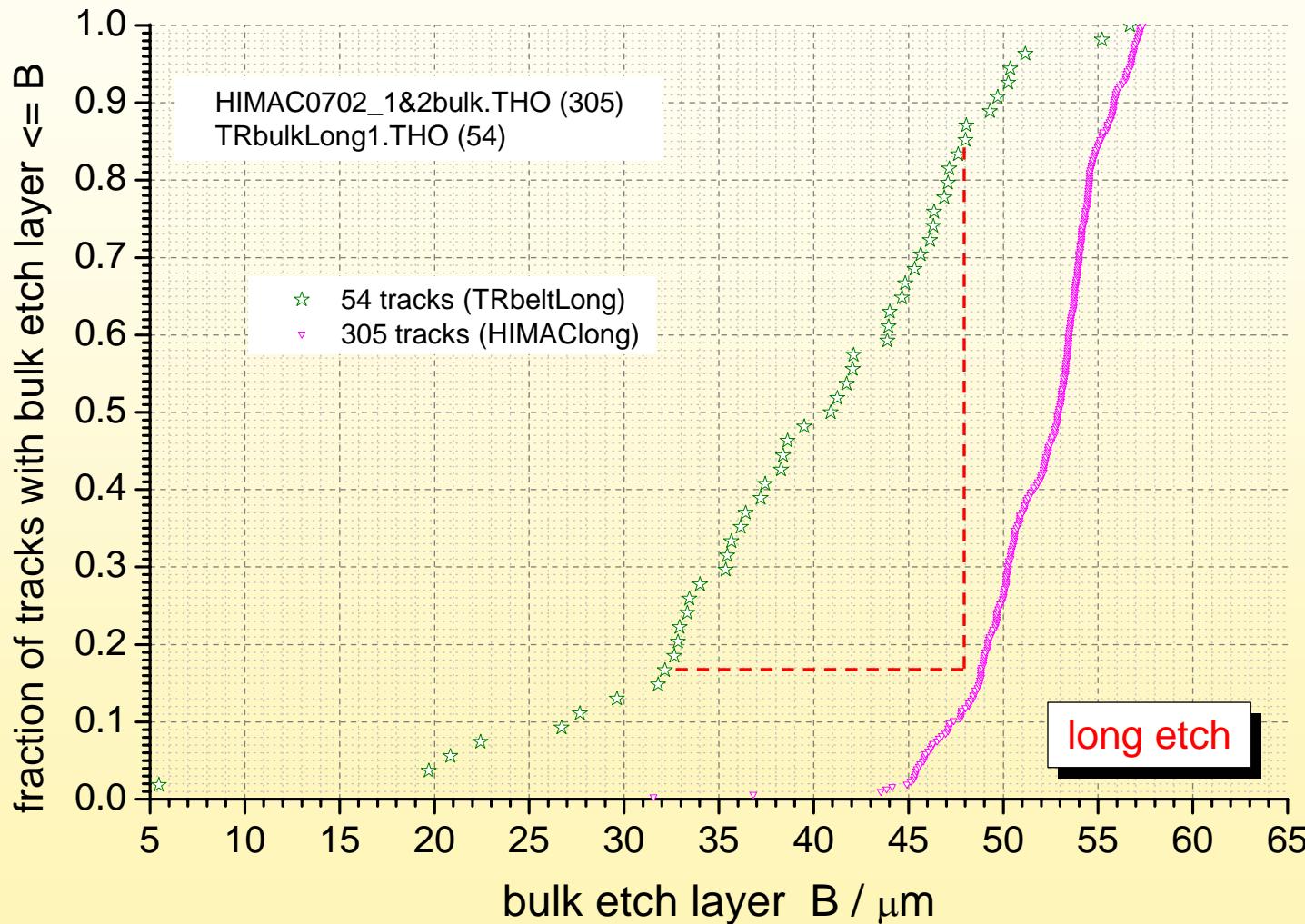
(CR 39, ISS mission/HIMAC)

Local bulk layer distributions short etch (CR 39)



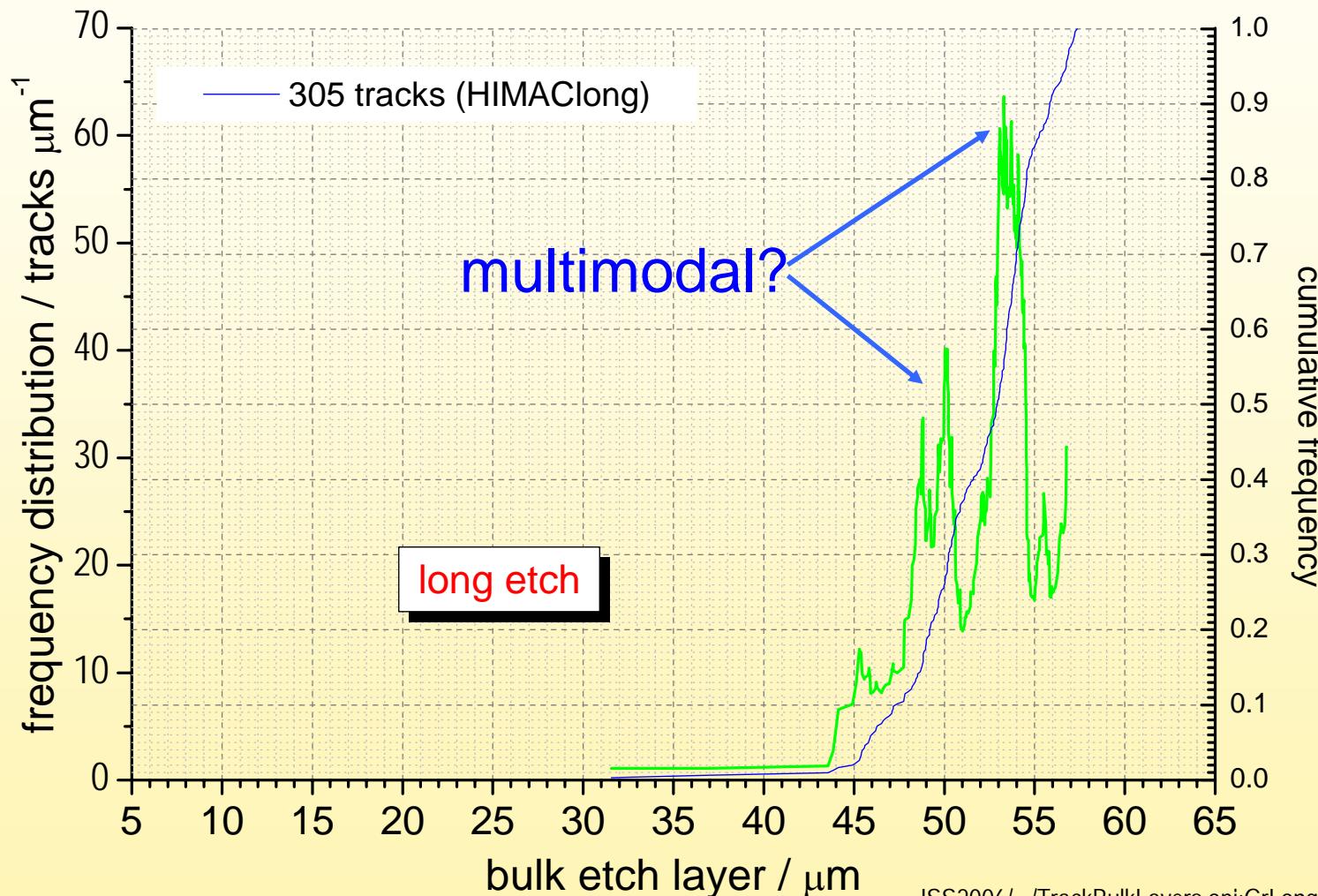
ISS2006/.../TrackBulkLayers.opj:GrShortA

Local bulk layer distributions long etch (CR39)



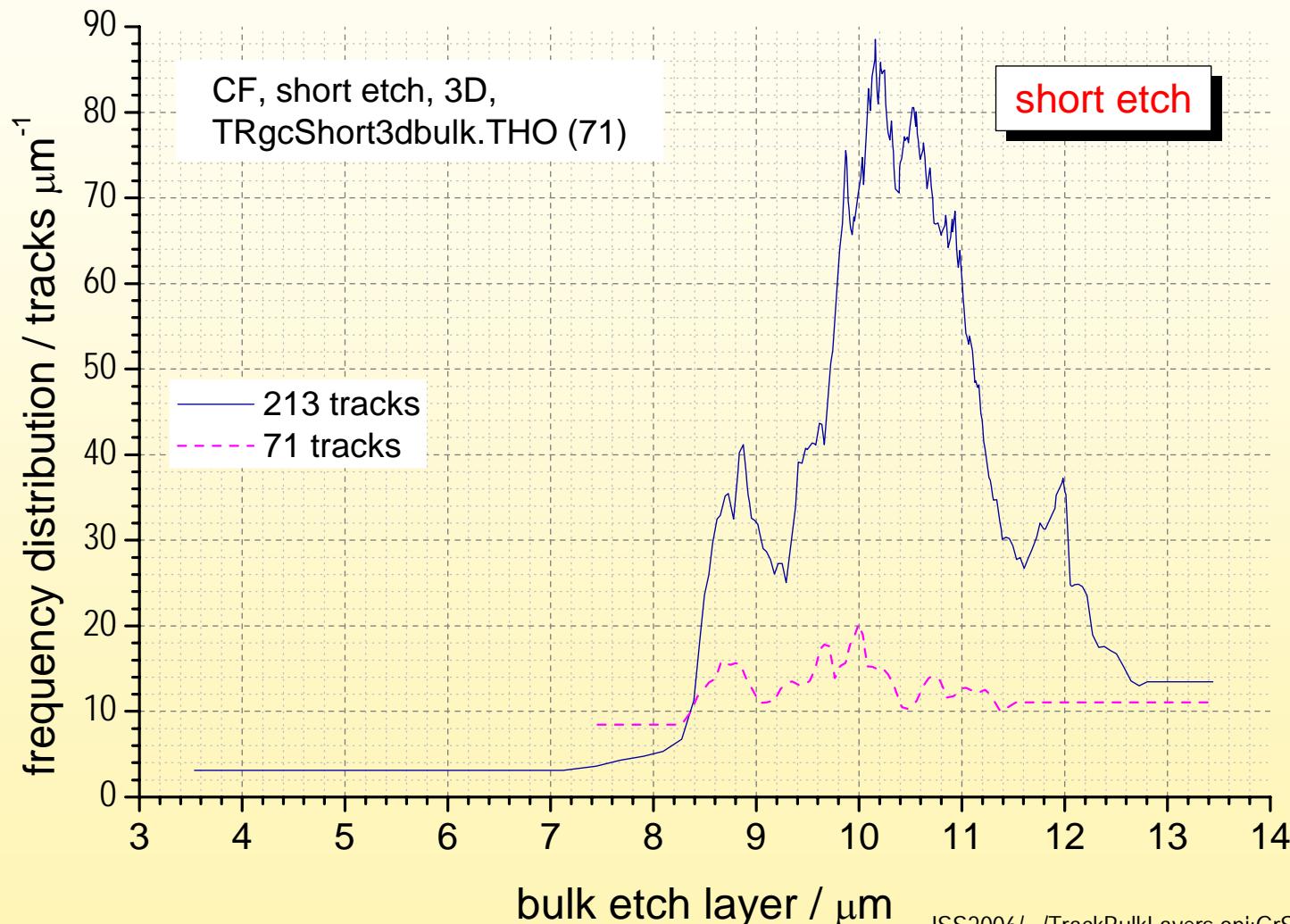
ISS2006/.../TrackBulkLayers.opj:GrLongA

Local bulk layer distributions long etch, accelerator only (CR 39)



ISS2006/.../TrackBulkLayers.opj:GrLongB

Local bulk layer distributions short etch, ISS and ground control (CR39)

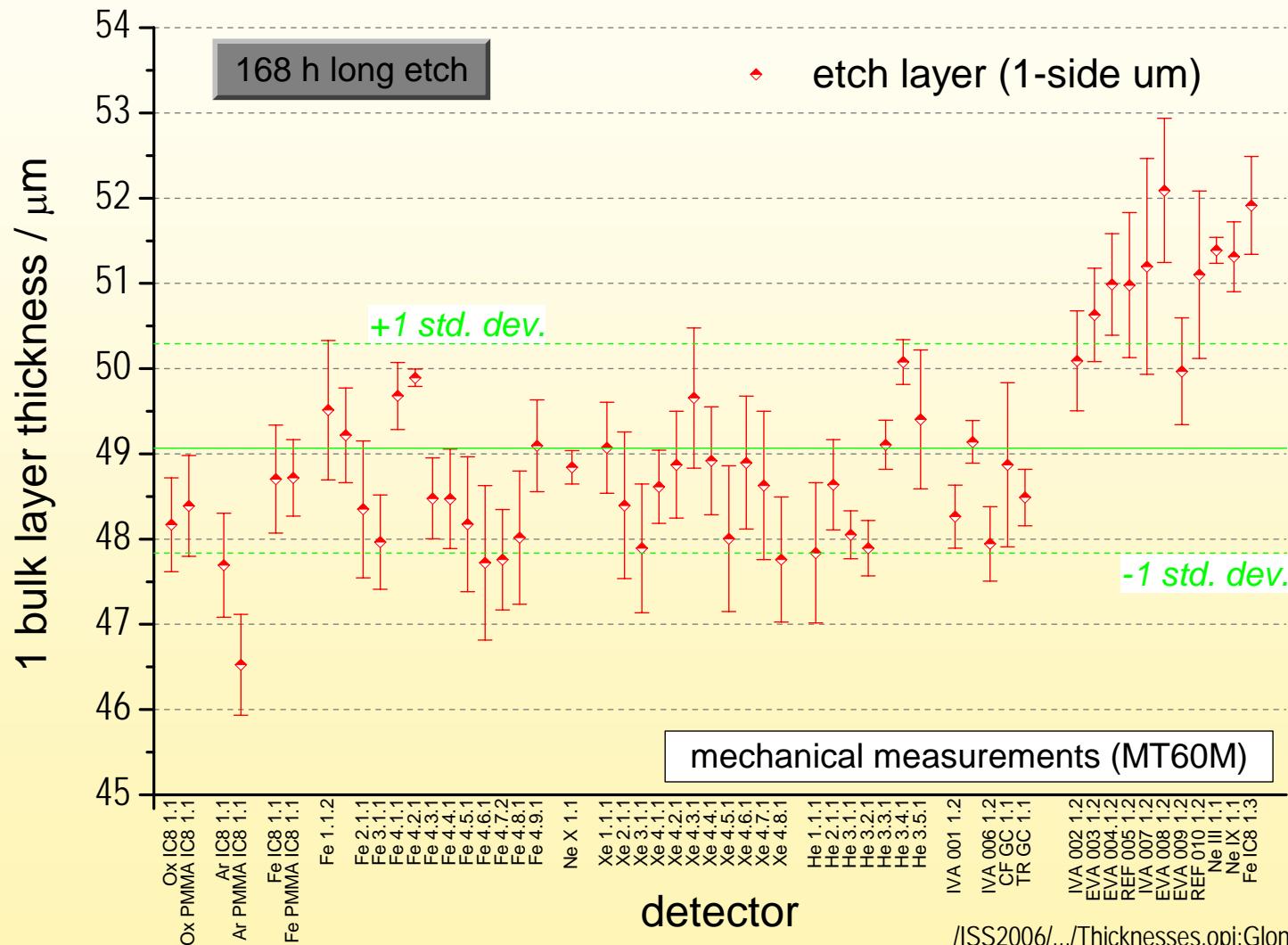


ISS2006/.../TrackBulkLayers.opj:GrShortB

global bulk layer data

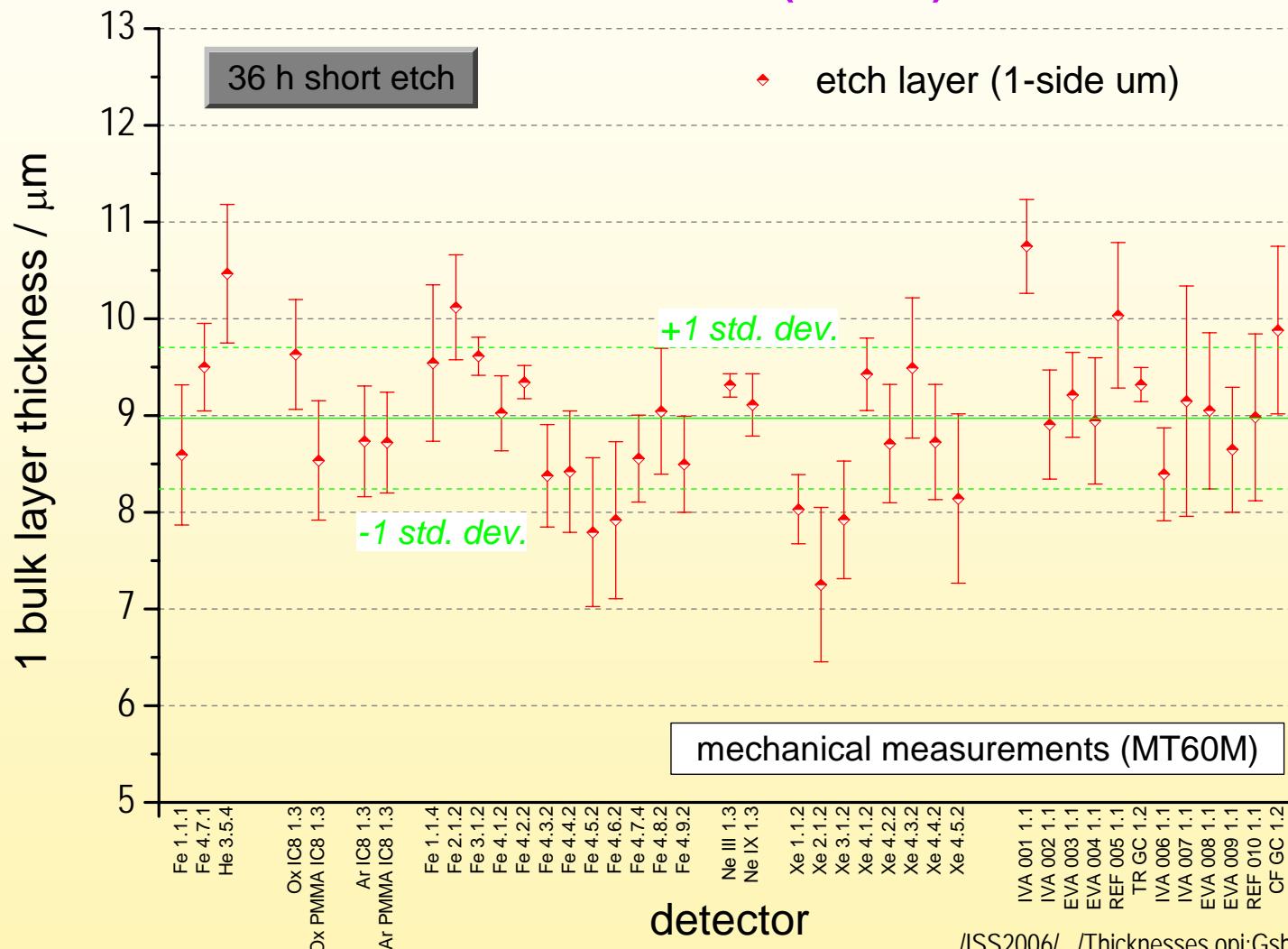
(CR 39, ISS mission/HIMAC
mechanical measurement)

Global bulk layer variation long etch data (CR 39)

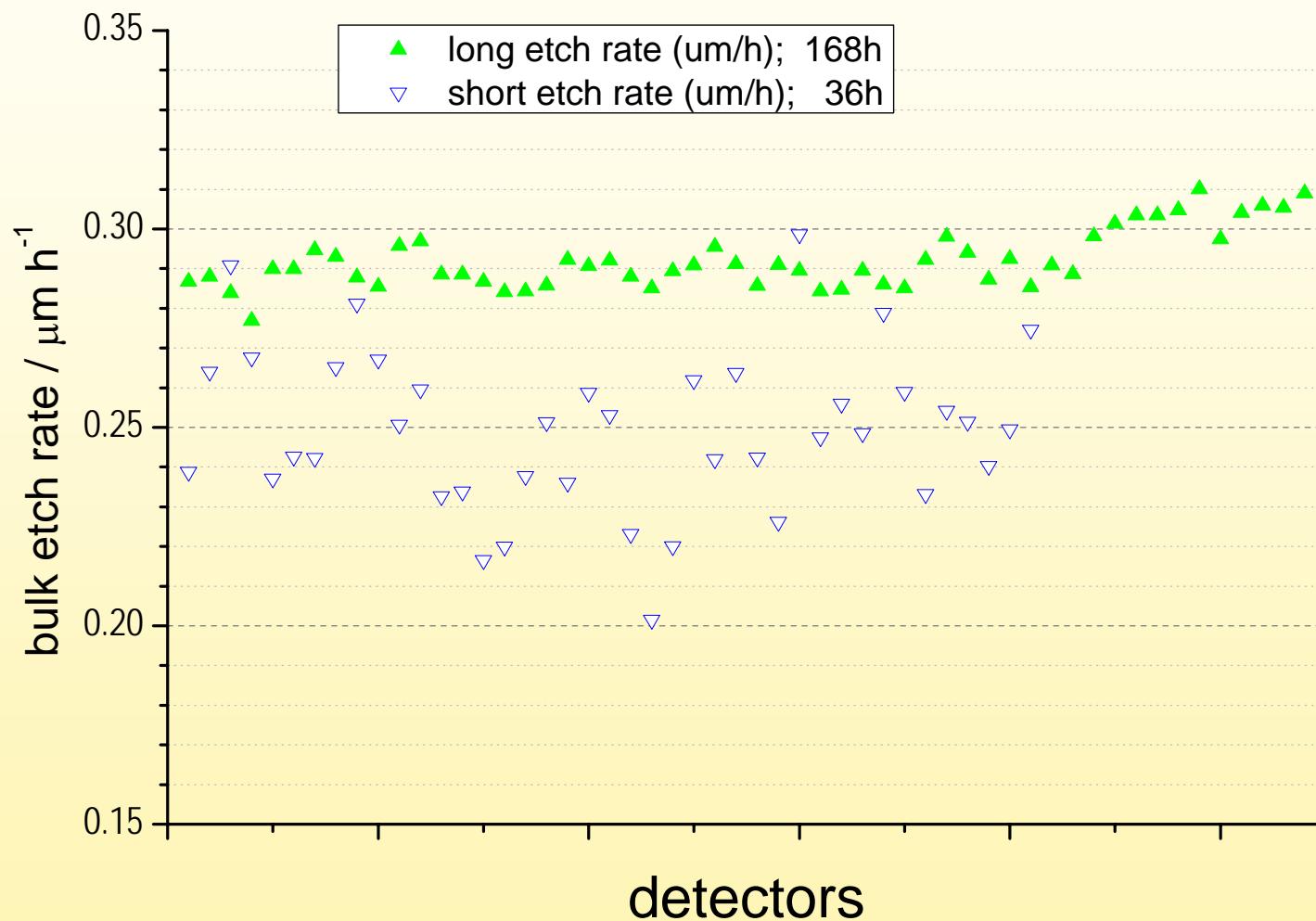


/ISS2006/.../Thicknesses.opj:GlongBulk

Global bulk layer variation short etch data (CR 39)



Global etch rate velocities - short etch versus long etch data (CR 39)



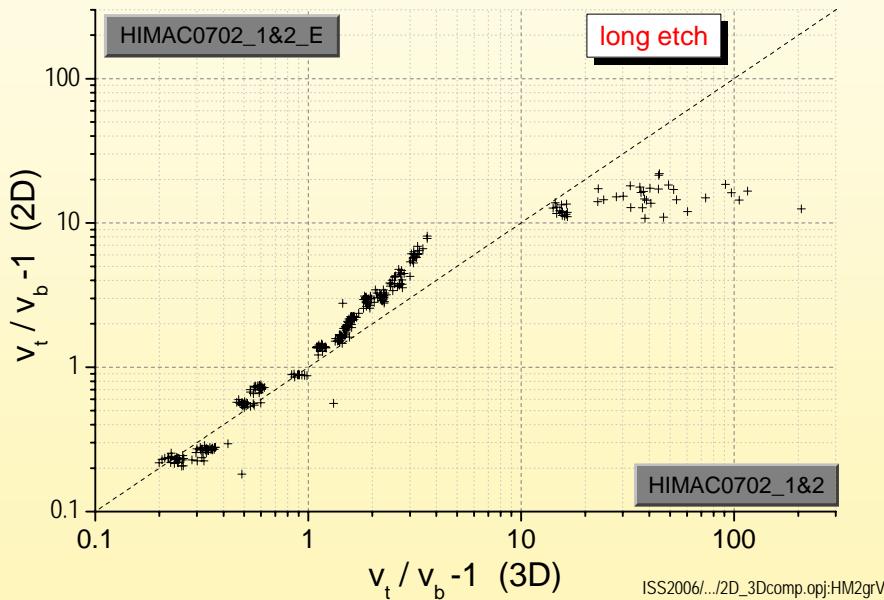
2D – 3D comparisons (CR 39)

Comparison excess etch rate and LET

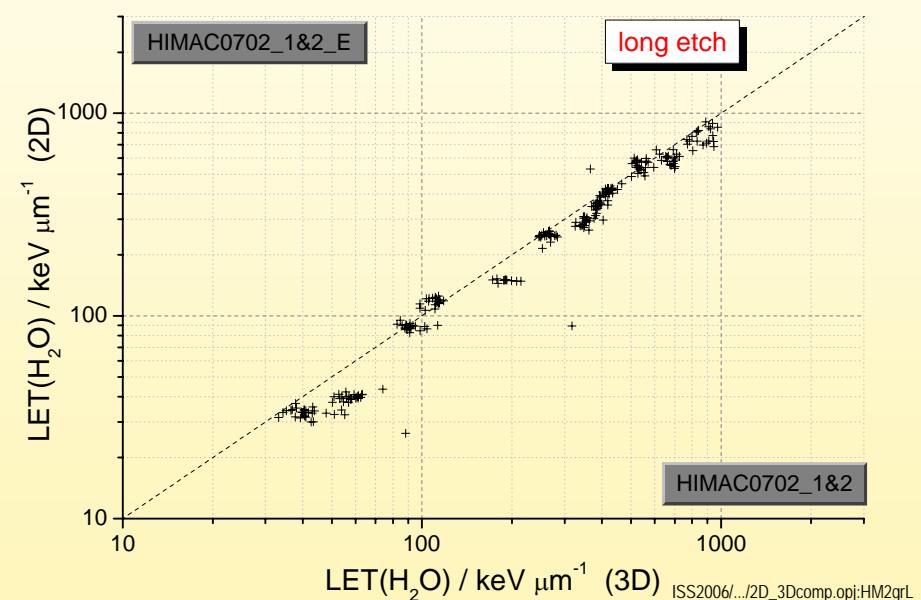
long etch (168h)

CR 39, accelerator calibration data

R-1



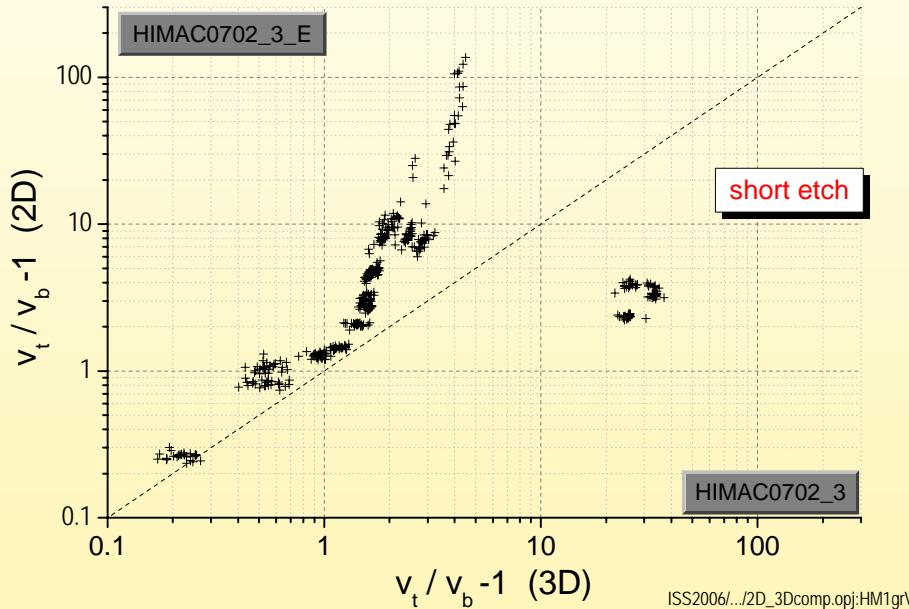
LET



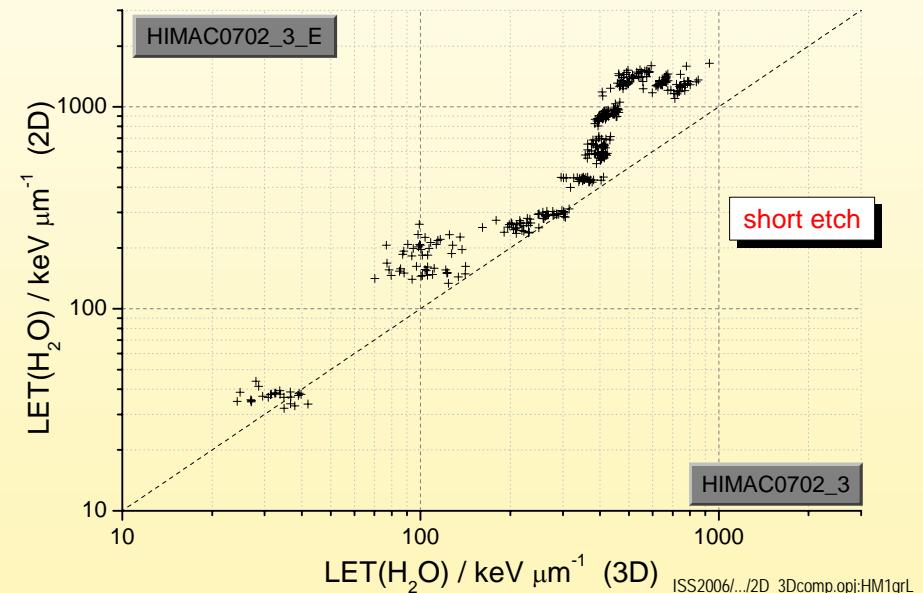
Comparison excess etch rate and LET short etch (36h)

CR 39, accelerator calibration data

R-1

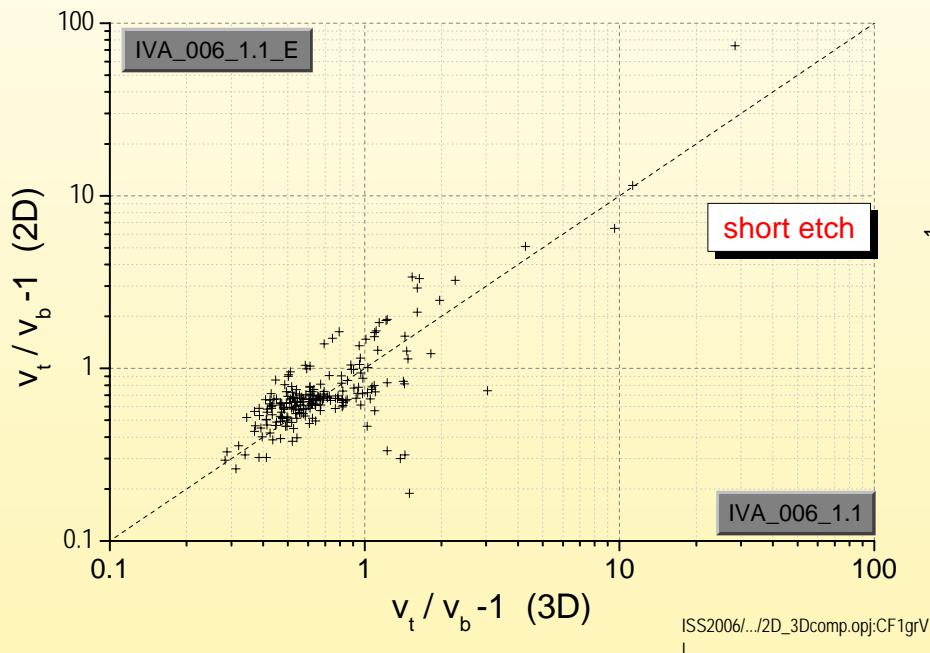


LET

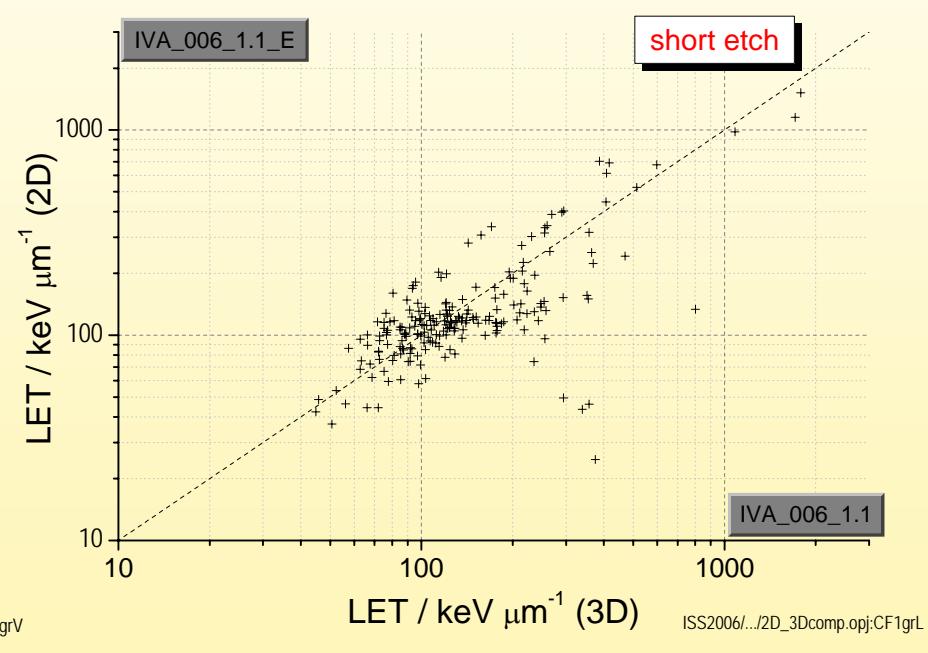


Comparison excess etch rate and LET short etch (36h) **CR 39, ISS exposure data**

R-1

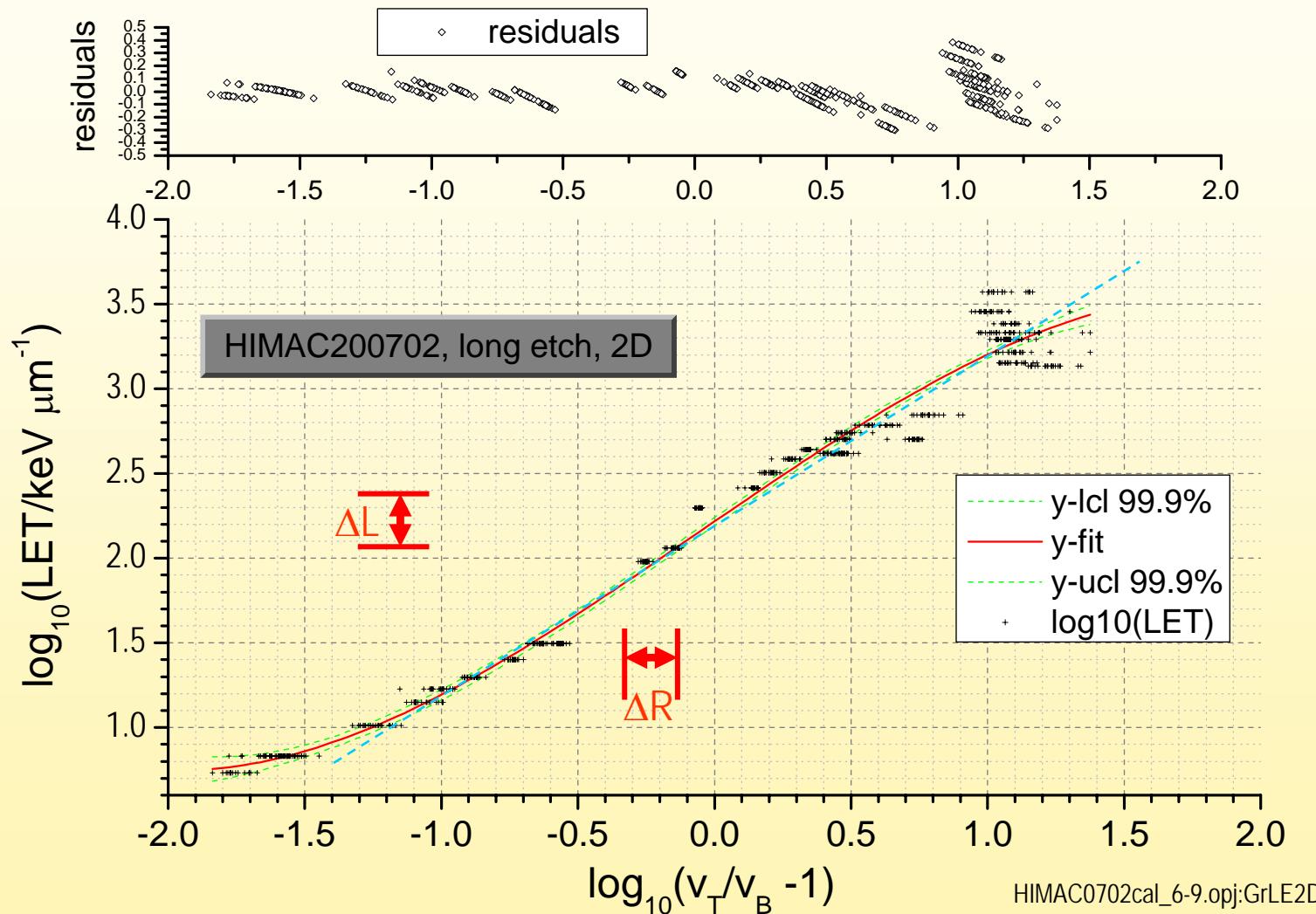


LET

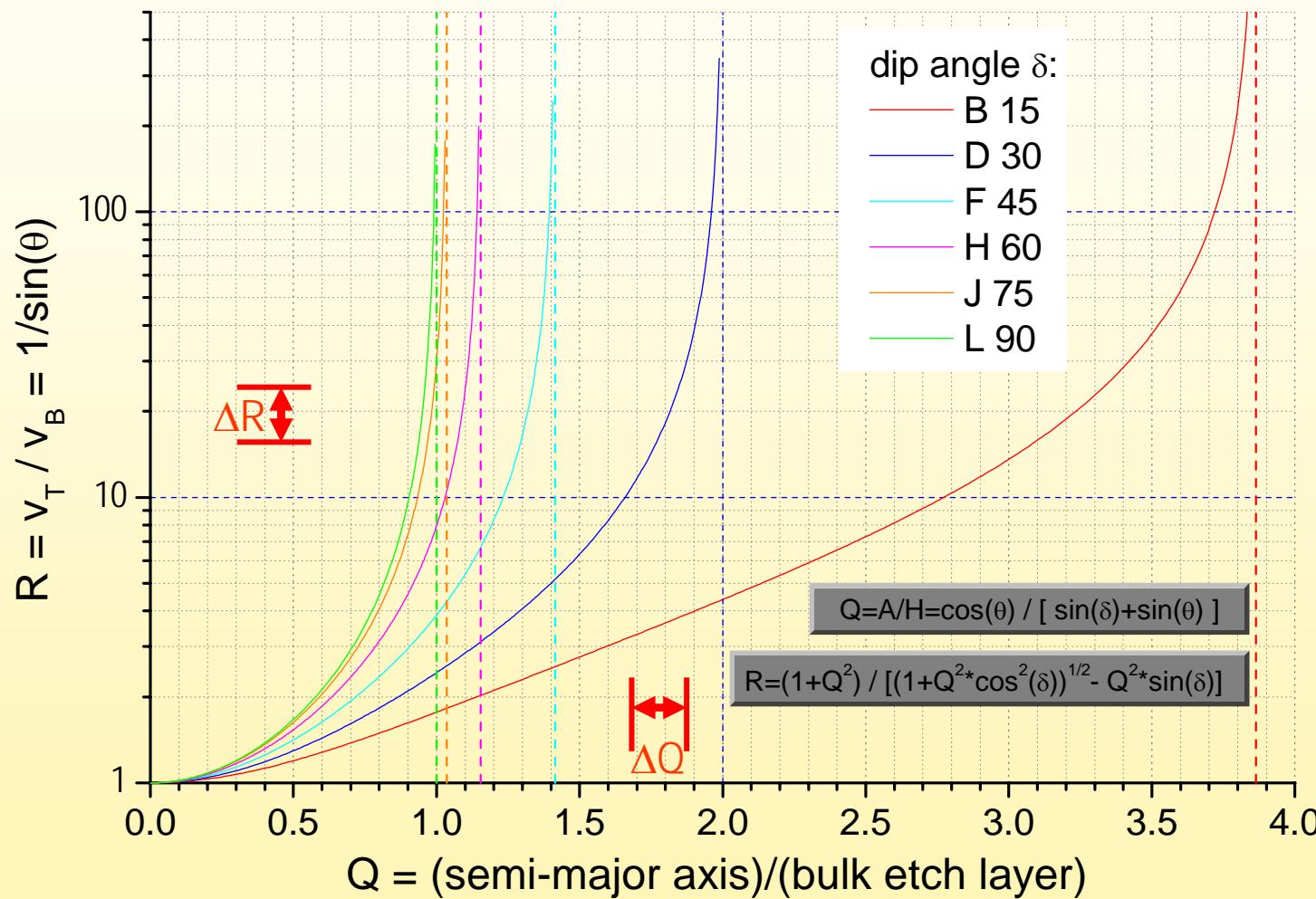


Implications for dosimetry

Calibration function LET(R)



Sensitivity analysis ΔR on ΔQ

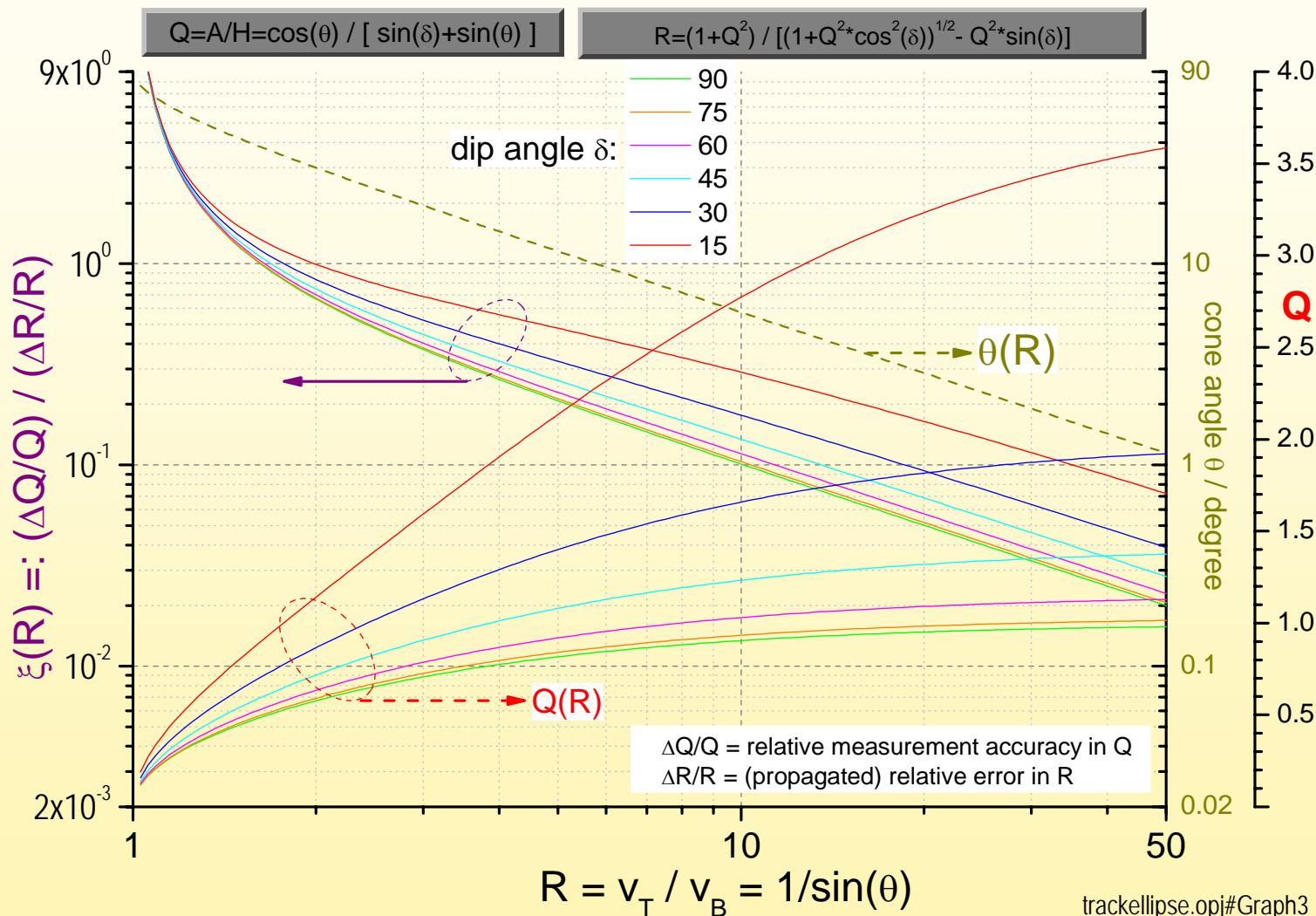


trackellipse.opj#Graph1

Case 1:

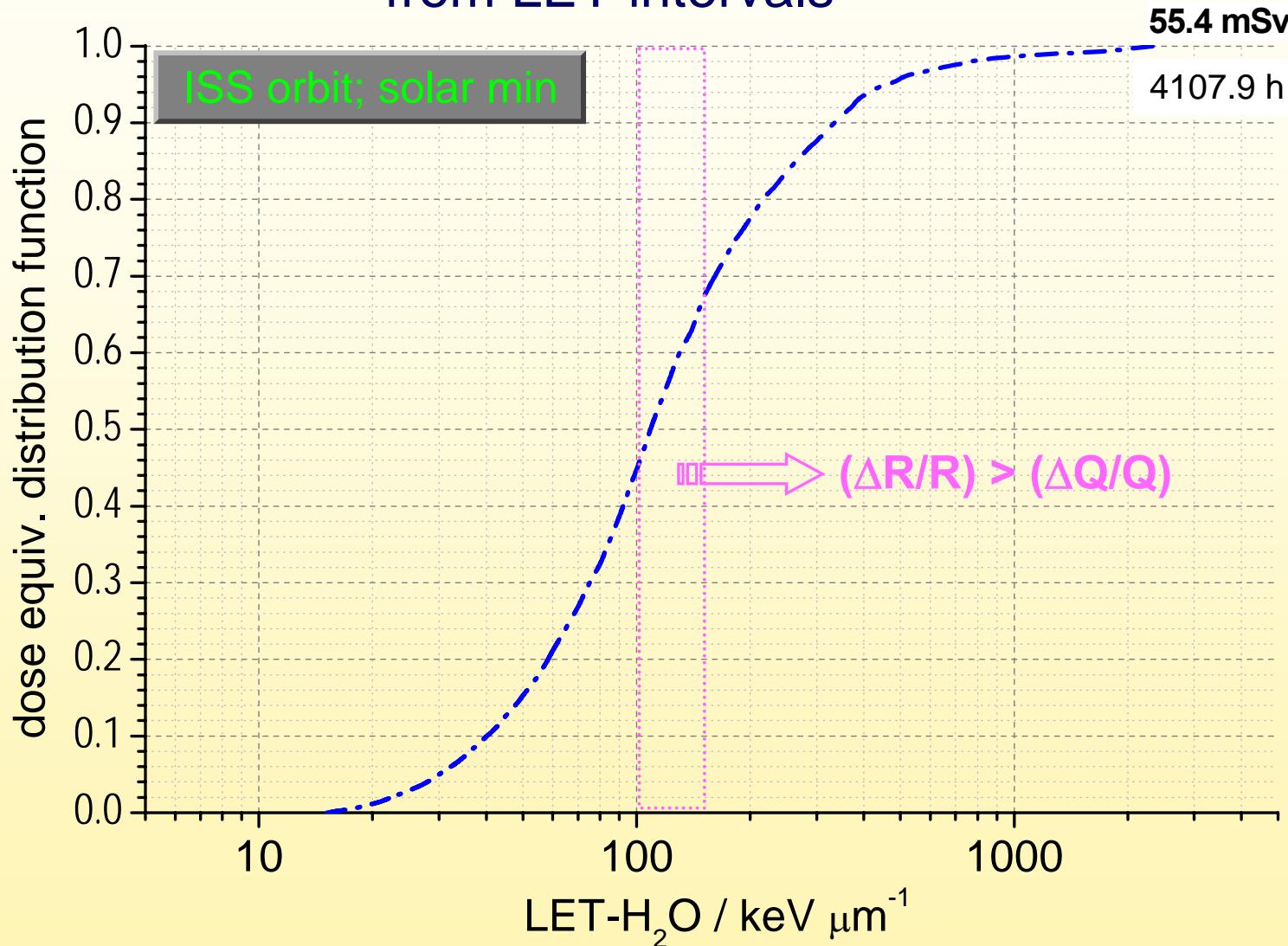
$\Delta Q/Q$ given, e.g. 20% =0.20

resulting $\Delta R/R = (\Delta Q/Q) / \xi = 0.20 / \xi$



trackellipse.opj#Graph3

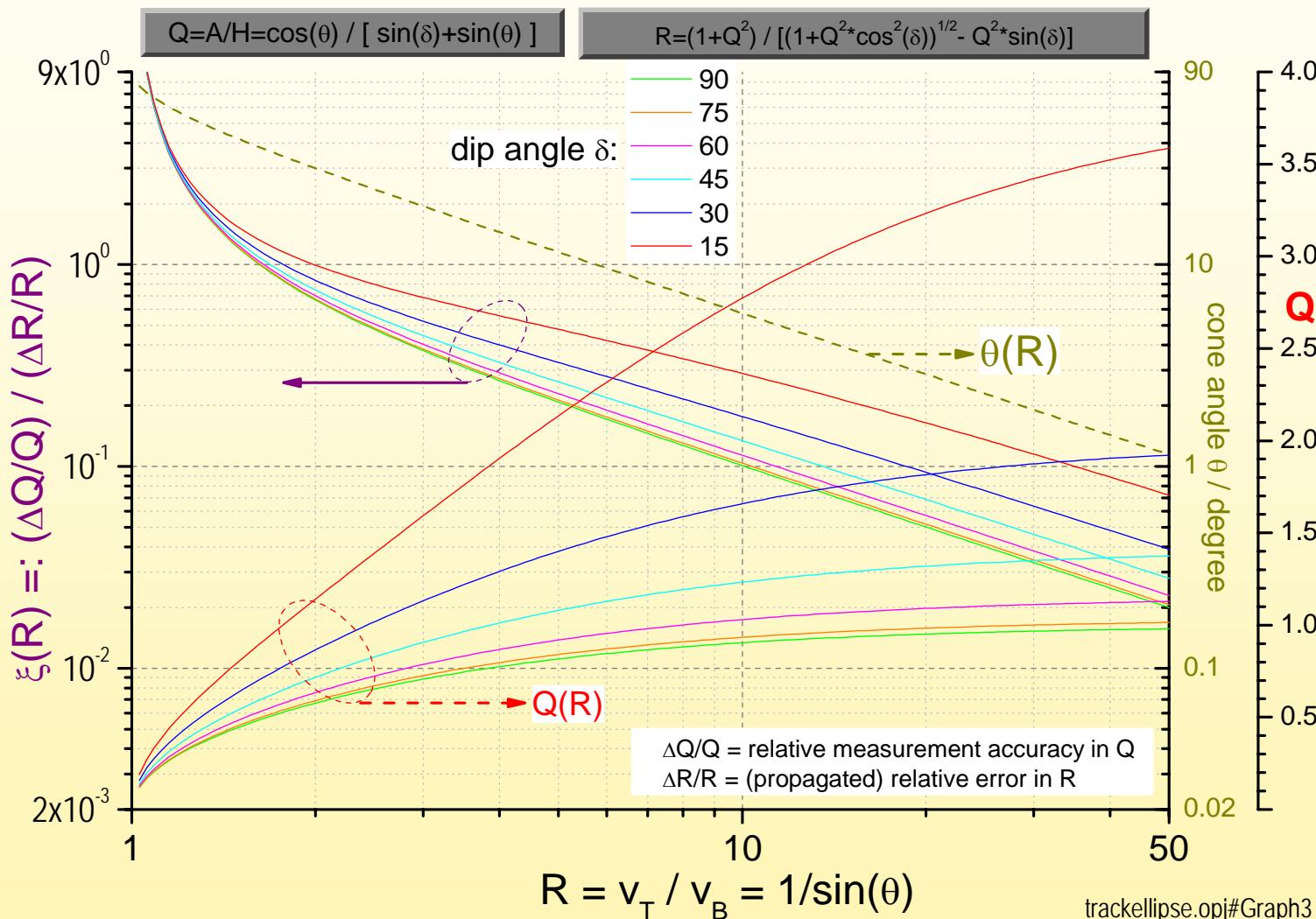
contributions to dose equivalent from LET intervals



Case 2:

$\Delta R/R$ prescribed, e.g. 20% = 0.20

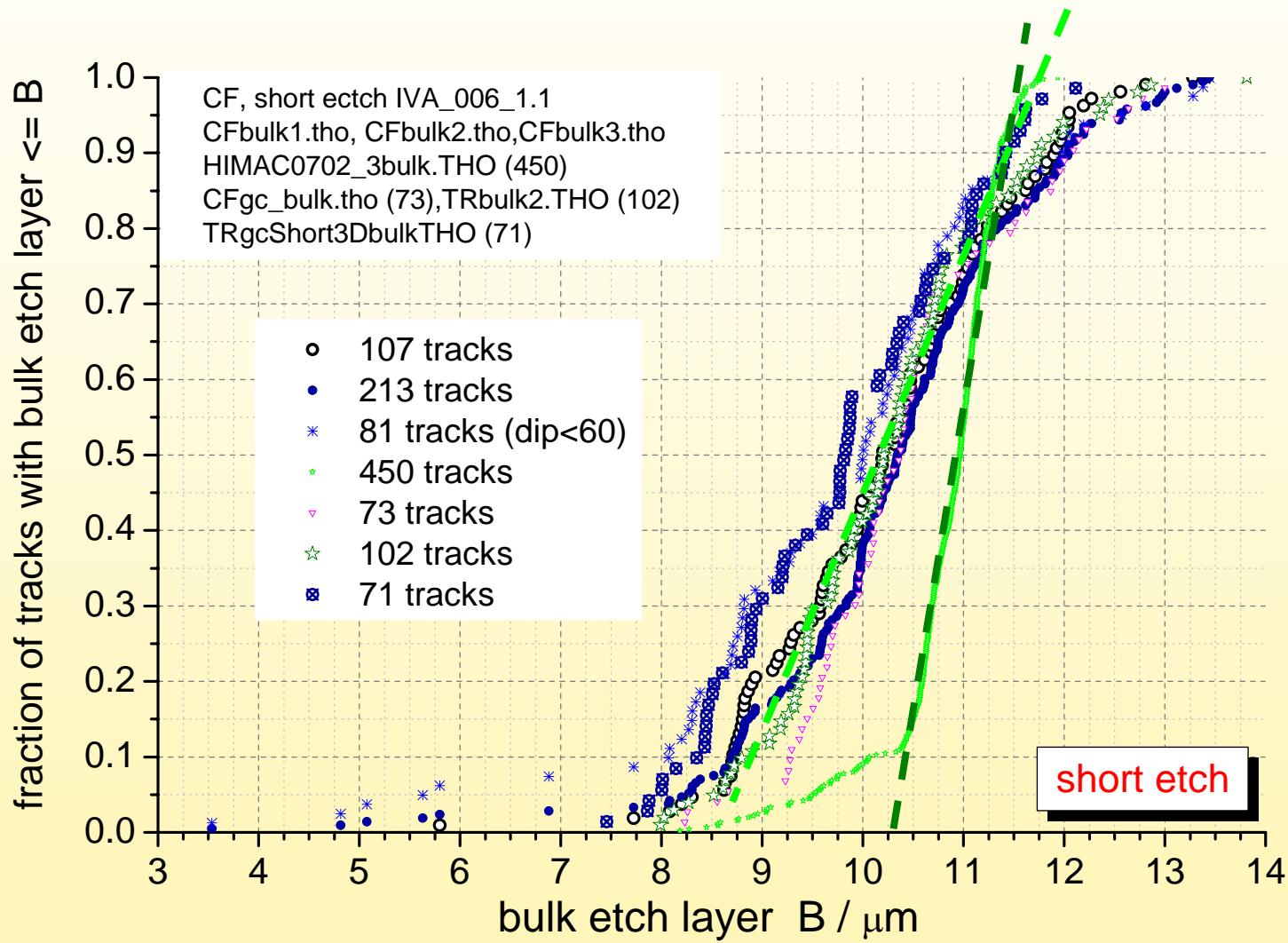
$$\text{required } \Delta Q/Q = (\Delta R/R) * \xi = 0.20 * \xi$$



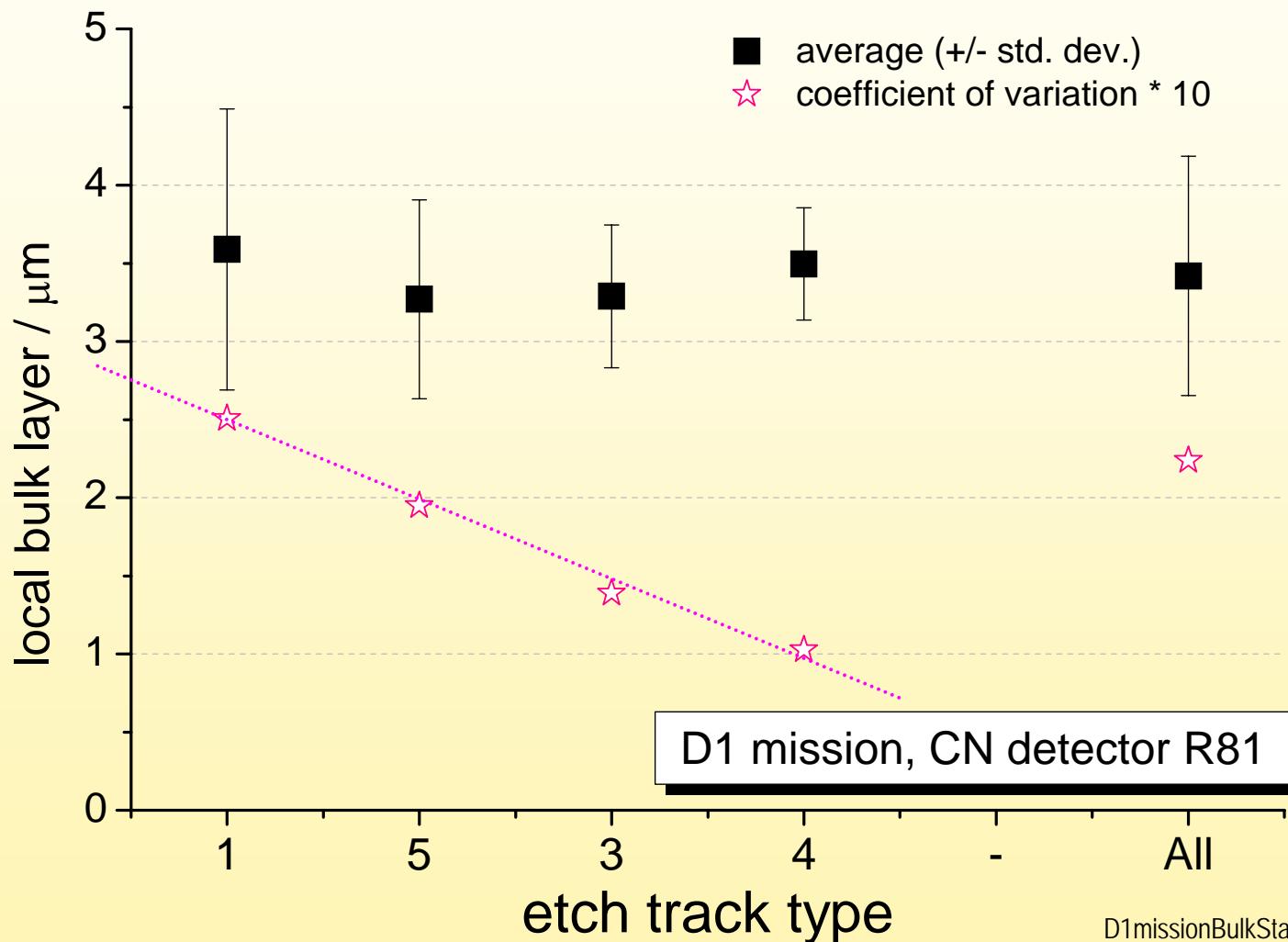
trackellipse.opj#Graph3

Puzzles

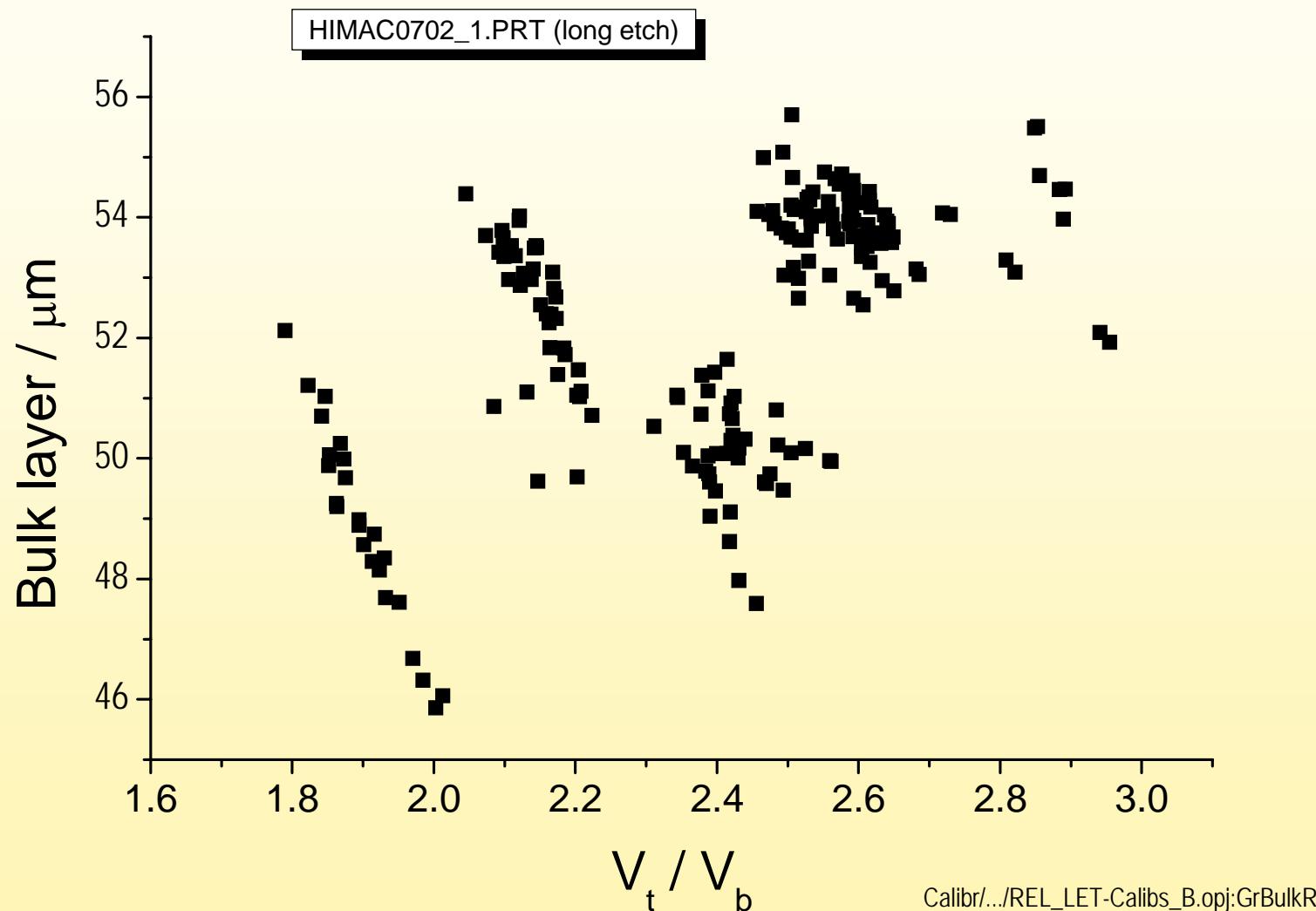
(a few, and for me)

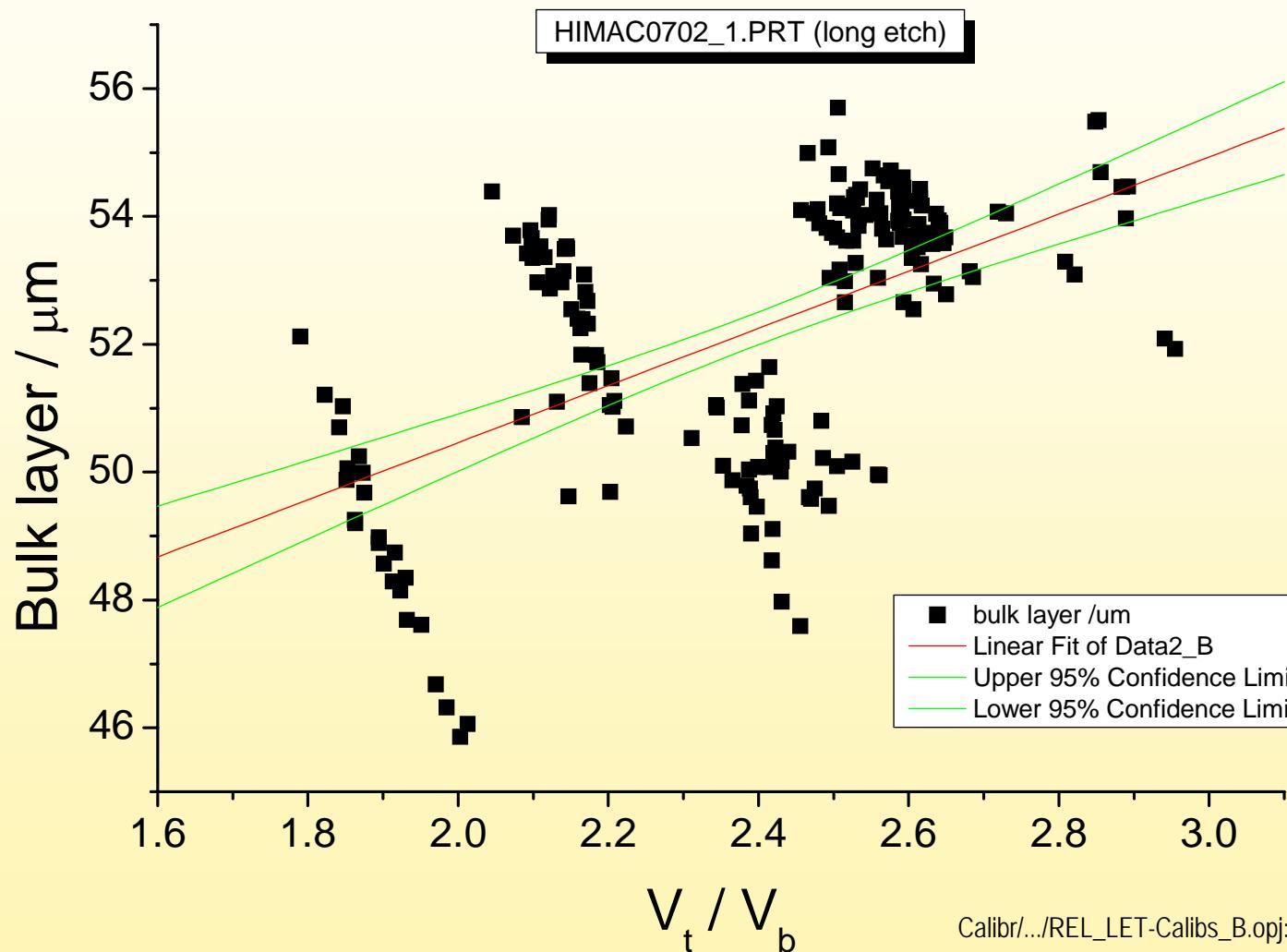


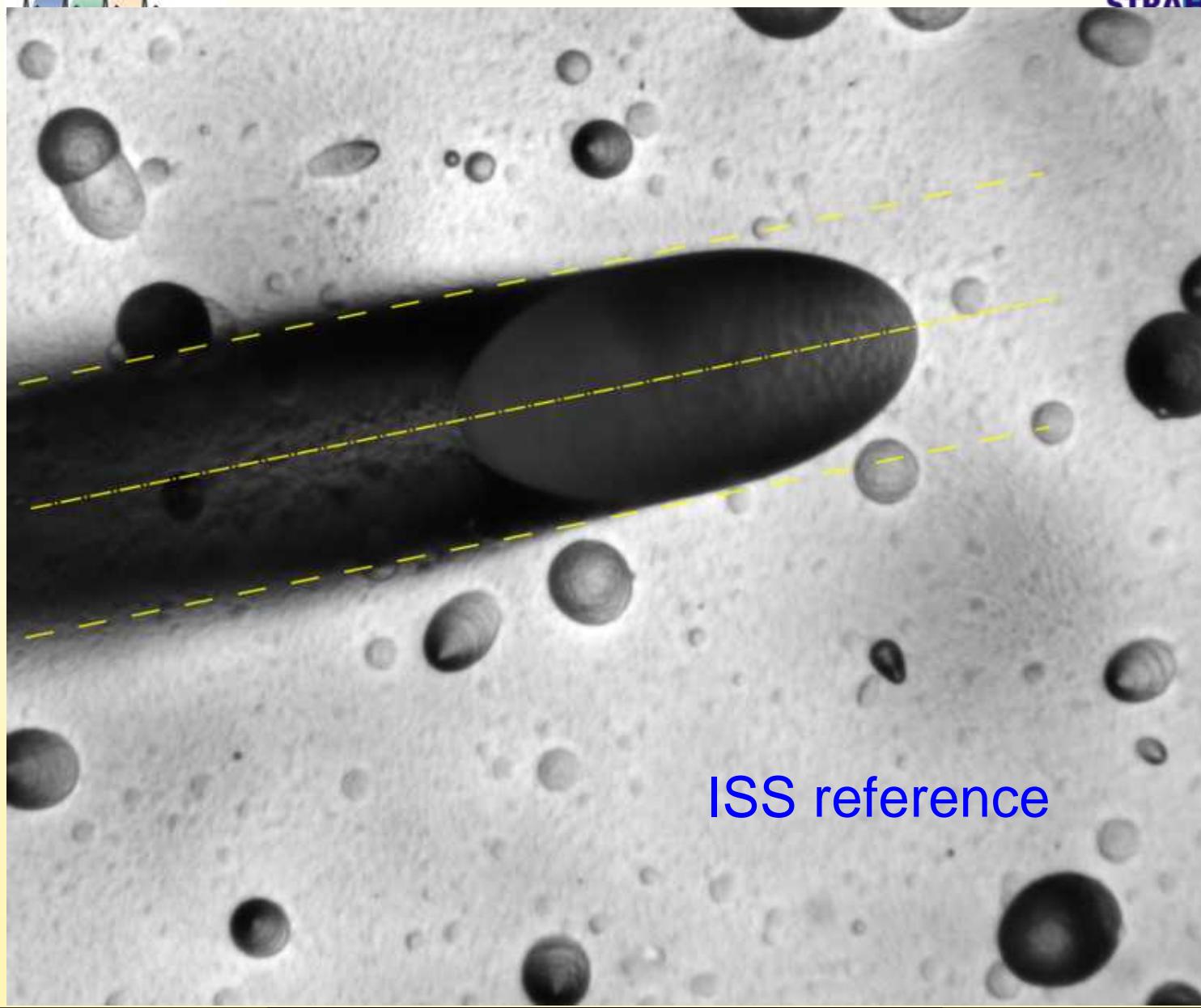
ISS2006/.../TrackBulkLayers.opj:GrShortA



D1missionBulkStatistics.opj







Summary and Conclusion

- Bulk etch rate in plastic detectors varies significantly
 - during etch time (CR 39)
 - locally by 10% to 25% (CR 39 and cellulose nitrate)
- Precision of dose equivalent measured thereby limited to perhaps 20% or more (neglecting other sources of error)

Overview

Historical background – motivation

2D measure

3D measure

3D measure

3D measure

Local bulk la

Local bulk la

Global bulk la

2D – 3D con

Implications for dosimetry

Puzzles (a few, for me)



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(local thickness)